

11th Overset Grid Symposium
October 15th-18th, 2012
Dayton, Ohio, USA



Common Aerospace Applications at DLR Utilizing the Overset Grid Capabilities of DLR's CFD Codes

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Knowledge for Tomorrow



Outline

- Methodology
 - DLR's solvers w/ overset grid capabilities
 - Our hole-cutting approaches
 - Chimera wall projection
 - Load integration
- Applications
 - CFD-6DoF
 - CROR
 - Helicopters
 - Control surface motion
 - Local discretisation improvement
 - Code-to-code coupling



Methodology



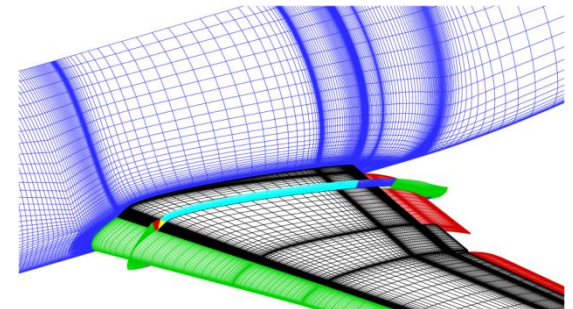
DLR's CFD Solvers w/ Overset Grid Capabilities

Common to both solvers:

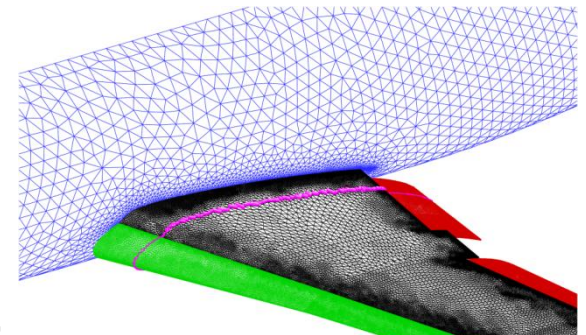
- Developments started in mid 1990s
- FV, 2nd order accuracy in space & time
- ALE capability
- Moving, deforming meshes
- Turbulence models: 1-eqn. SA variants, 2-eqn. k- ω -type models, EARSM, RSM; DES, LES
- Fluxes: Central+scalar/matrix diss., Upwinding
- Steady time int.: RK (FLOWer/TAU), LU-SGS, line-implicit (TAU) + multigrid
- Unsteady time int.: Dual-time stepping
- Hybrid MPI/OpenMP-based parallelisation

Special to TAU:

- Work horse of Airbus for aerodynamics analysis on unstructured meshes
- Python interfaces => scripting, in-memory data exchange (6DoF, CFD-CSM coupl.)
- Feature & adjoint-based adaptation



Multiblock-structured compressible RANS solver **FLOWer**

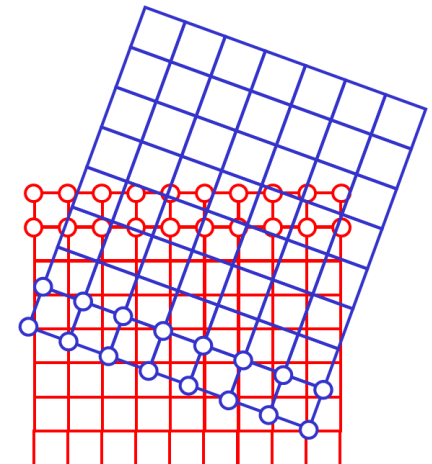


Unstructured compressible RANS solver **TAU**



Our Overset Grid Interpolation Technique

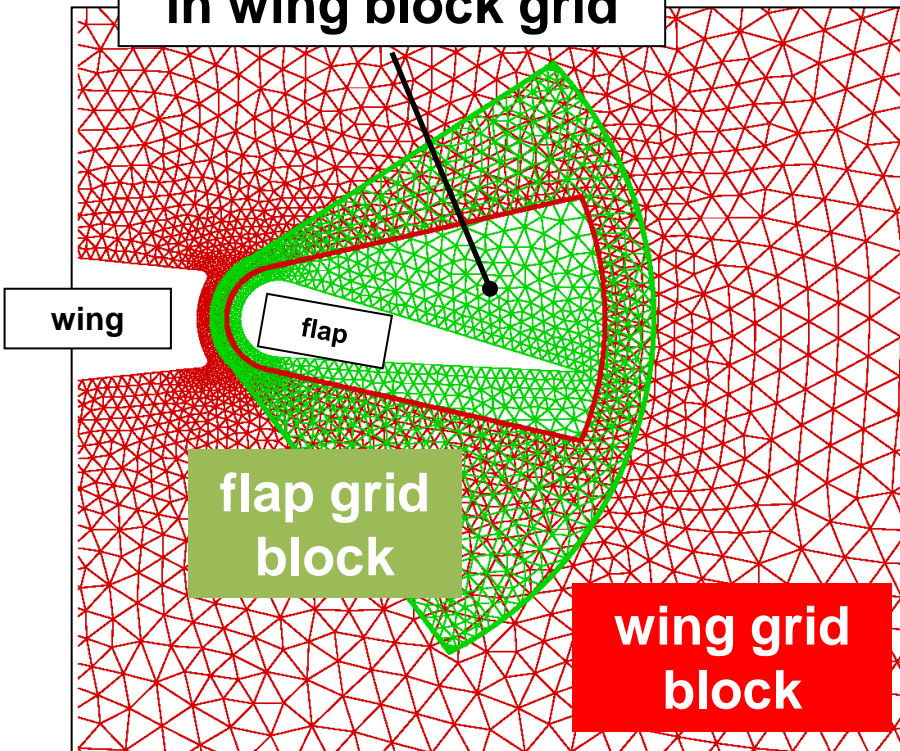
- Parallel donor search integrated directly in solver loop (no external tool, no file I/O); 2-stage search
 1. ADT-based search
 2. Iso-parametric mapping based search
- Interpolation is based on primary mesh cells using FE shape functions
 - Only 4 different FE shape functions need to be considered
 - Dual mesh contains arbitrary polyhedrons which would make interpolation more complex & expensive
- Interpolation takes place only on finest multigrid level
- 2 fringe layers



Our Hole-Cutting Strategies

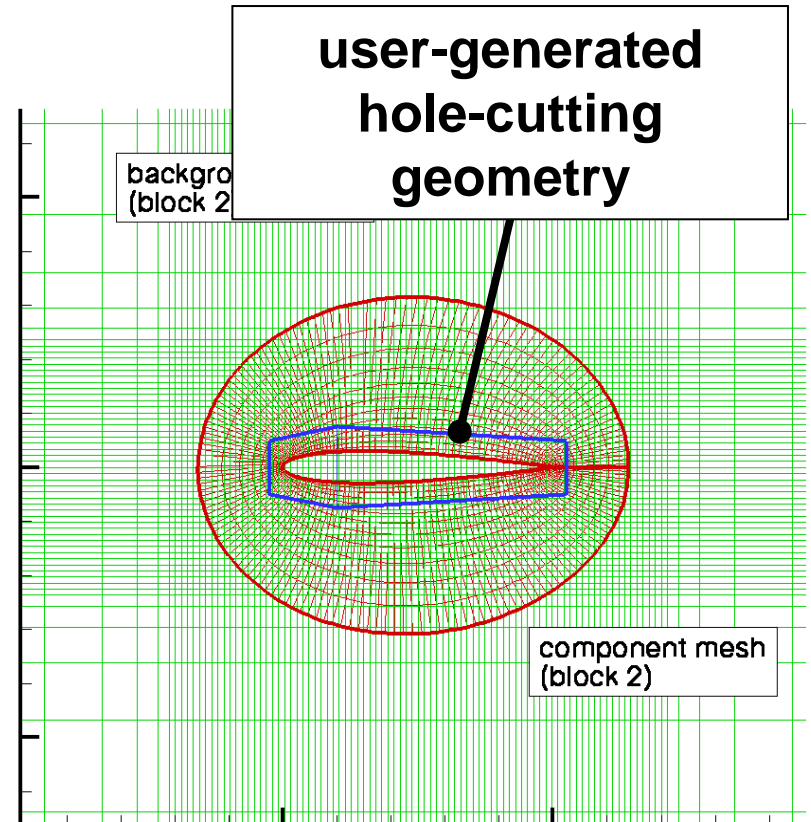
NO hole-cutting

pre-generated* hole
in wing block grid



Semi-automatic hole-cutting

user-generated
hole-cutting
geometry



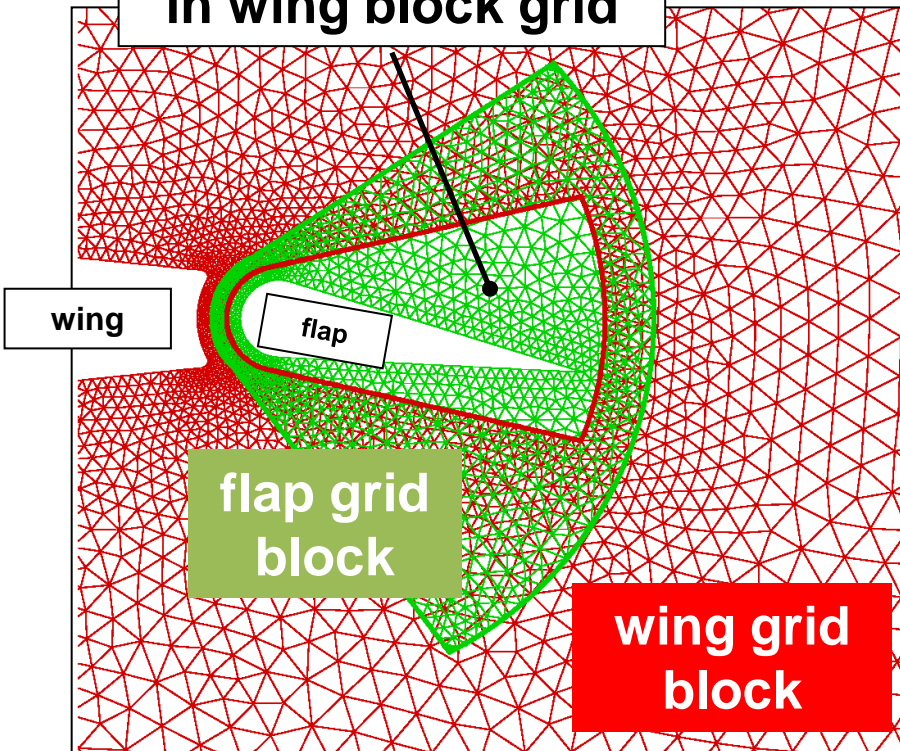
*generated during mesh
generation



Our Hole-Cutting Strategies

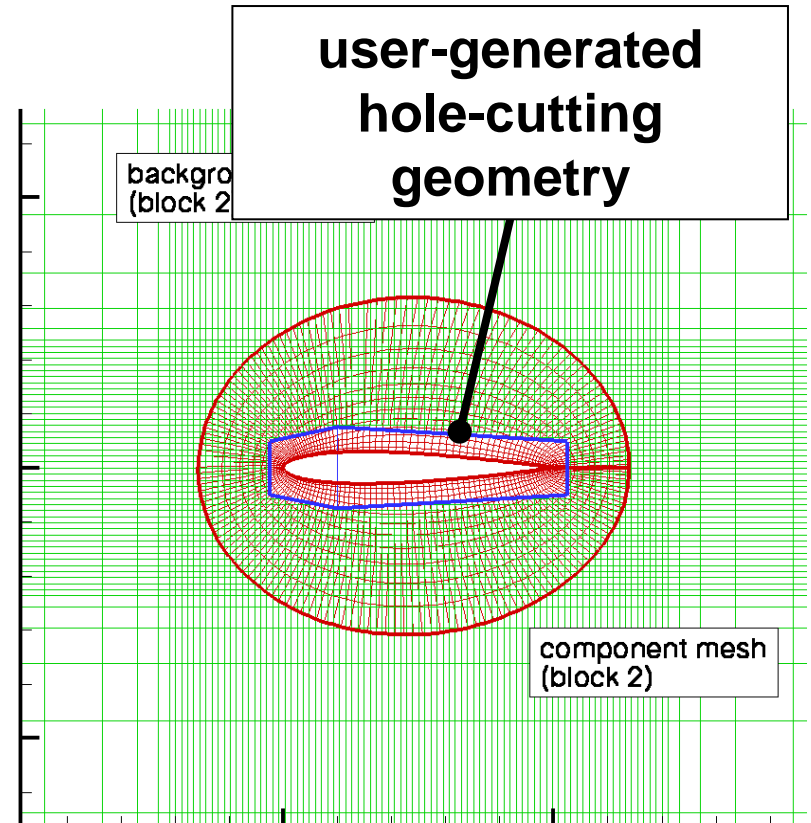
NO hole-cutting

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Semi-automatic hole-cutting

user-generated
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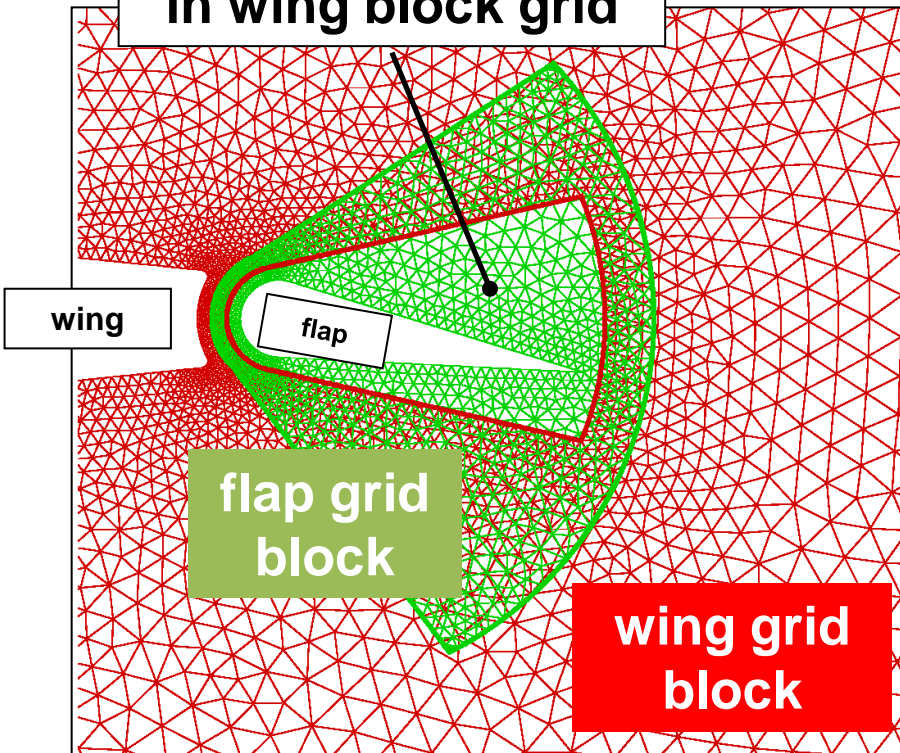
*generated during mesh
generation



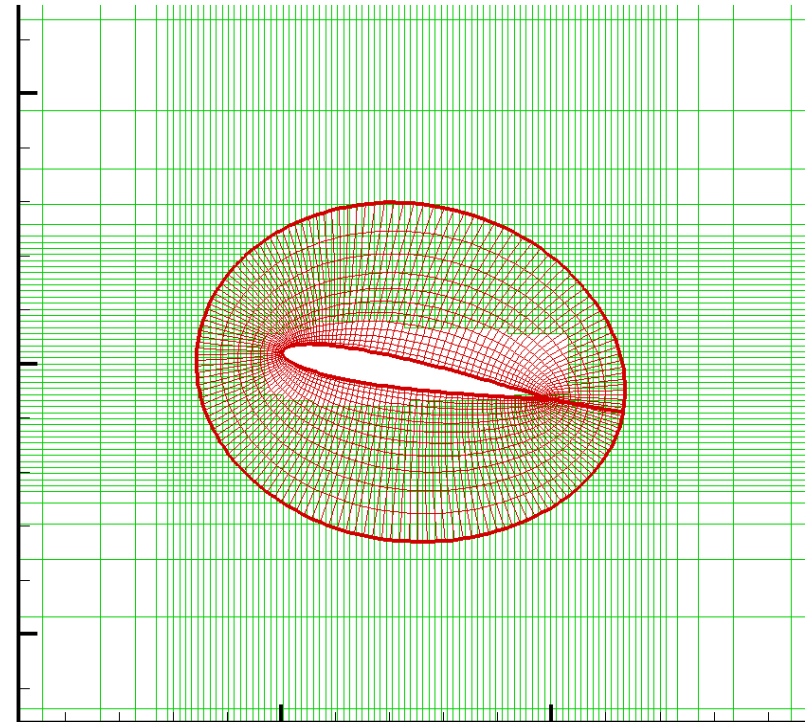
Our Hole-Cutting Strategies

NO hole-cutting

pre-generated* hole
in wing block grid



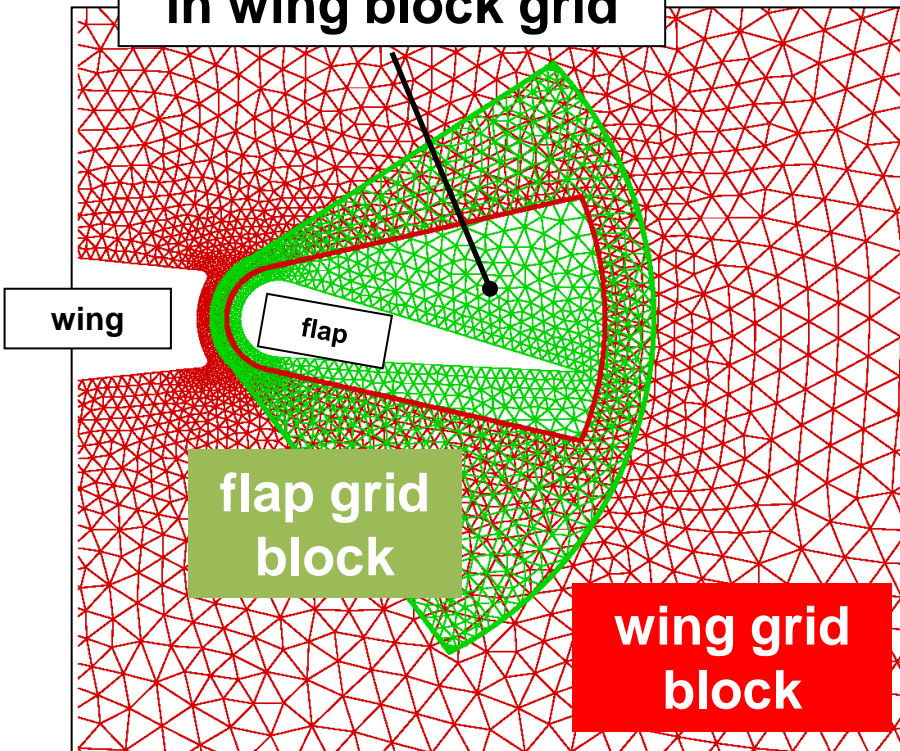
Semi-automatic hole-cutting



Our Hole-Cutting Strategies

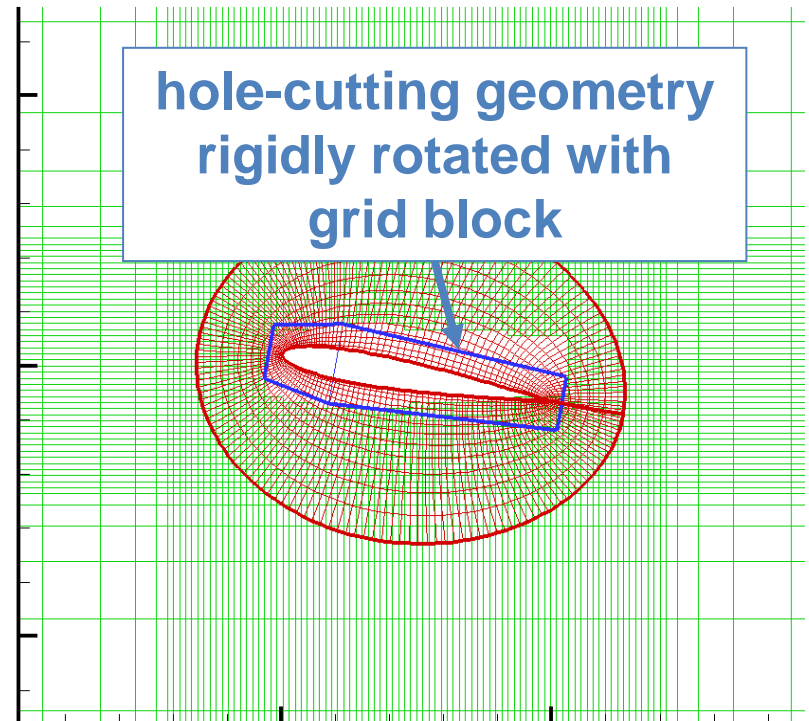
NO hole-cutting

pre-generated* hole
in wing block grid



Semi-automatic hole-cutting

hole-cutting geometry
rigidly rotated with
grid block



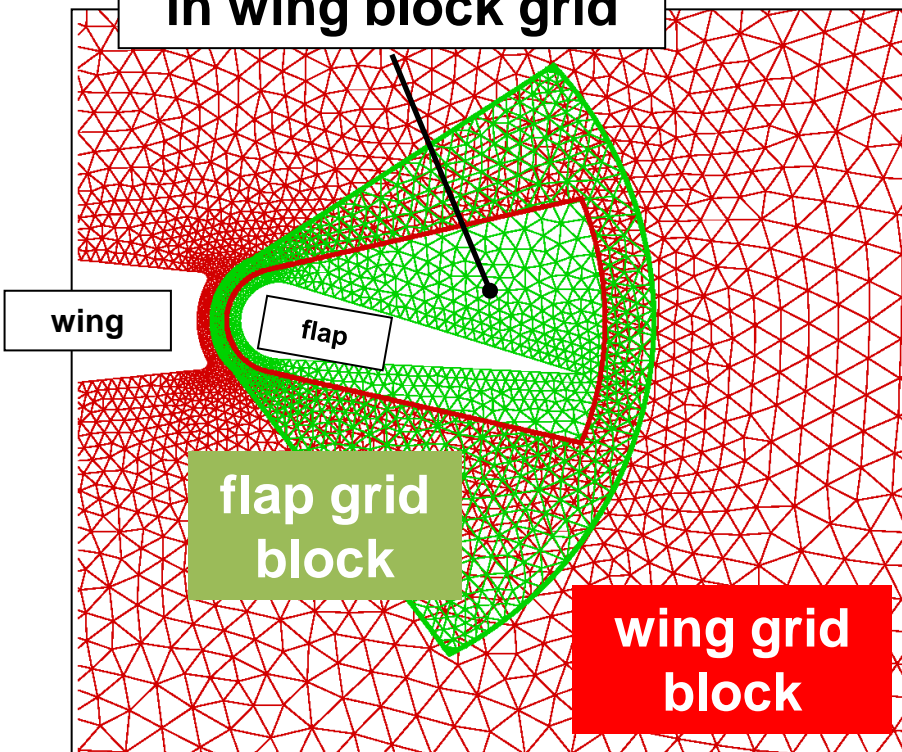
*generated during mesh
generation



Our Hole-Cutting Strategies

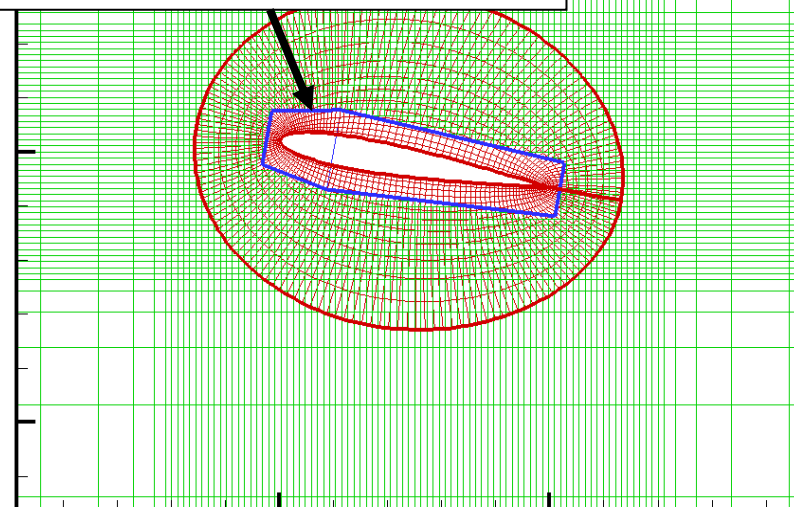
NO hole-cutting

pre-generated* hole
in wing block grid



Semi-automatic hole-cutting

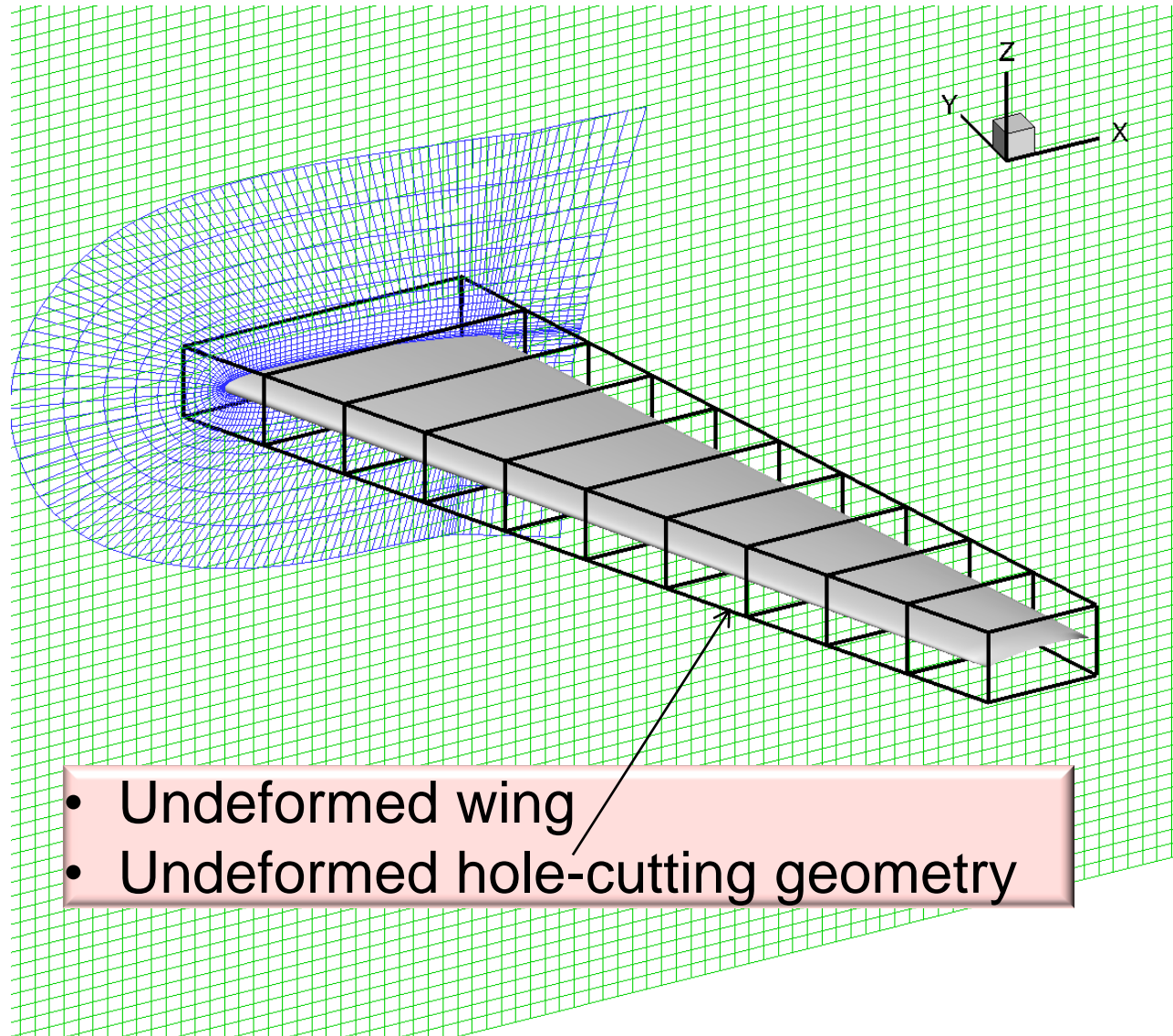
blanking recomputed
from rotated hole-
cutting geo



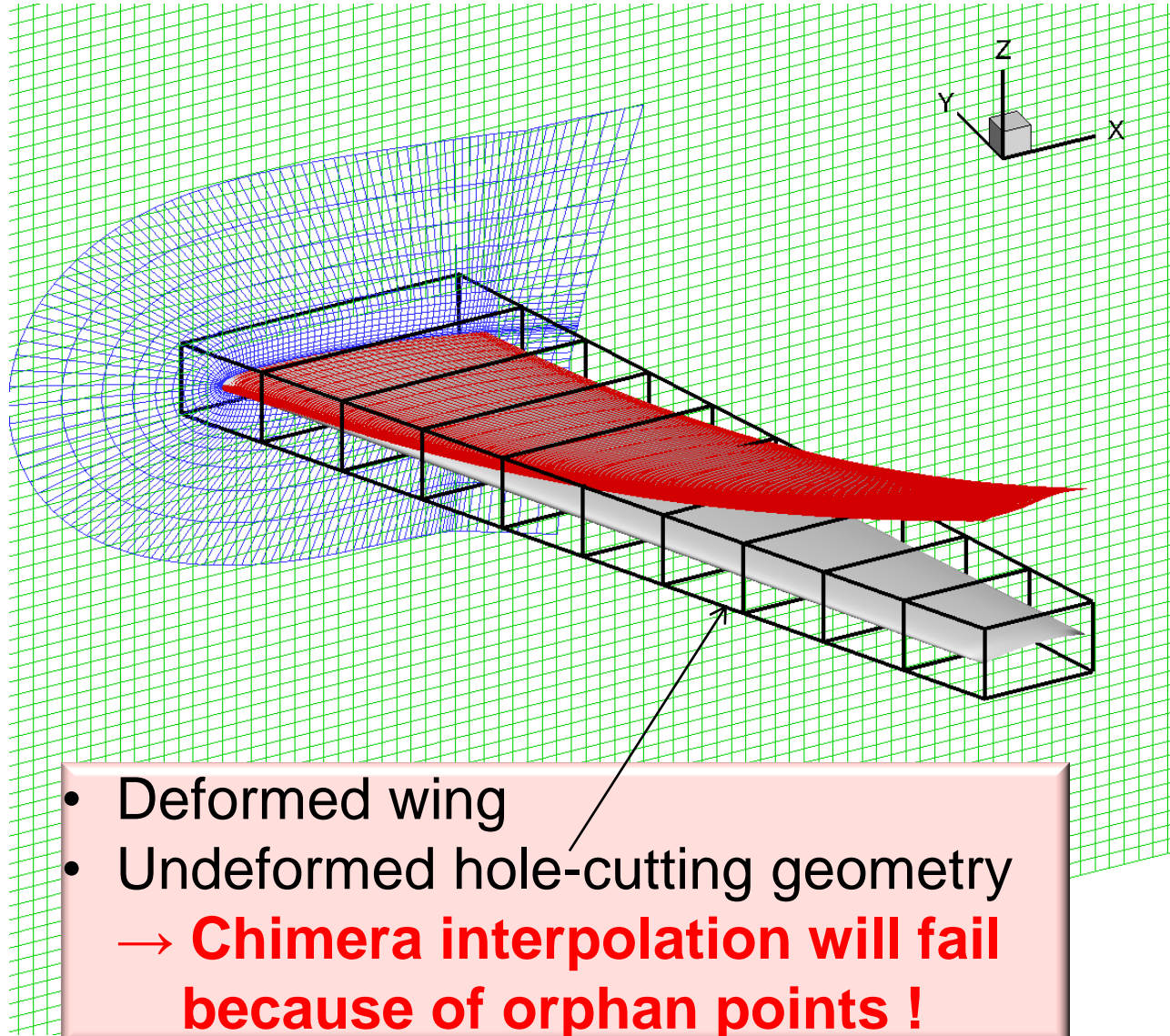
*generated during mesh
generation



Hole-Cutting Geometries & Mesh Deformation ?

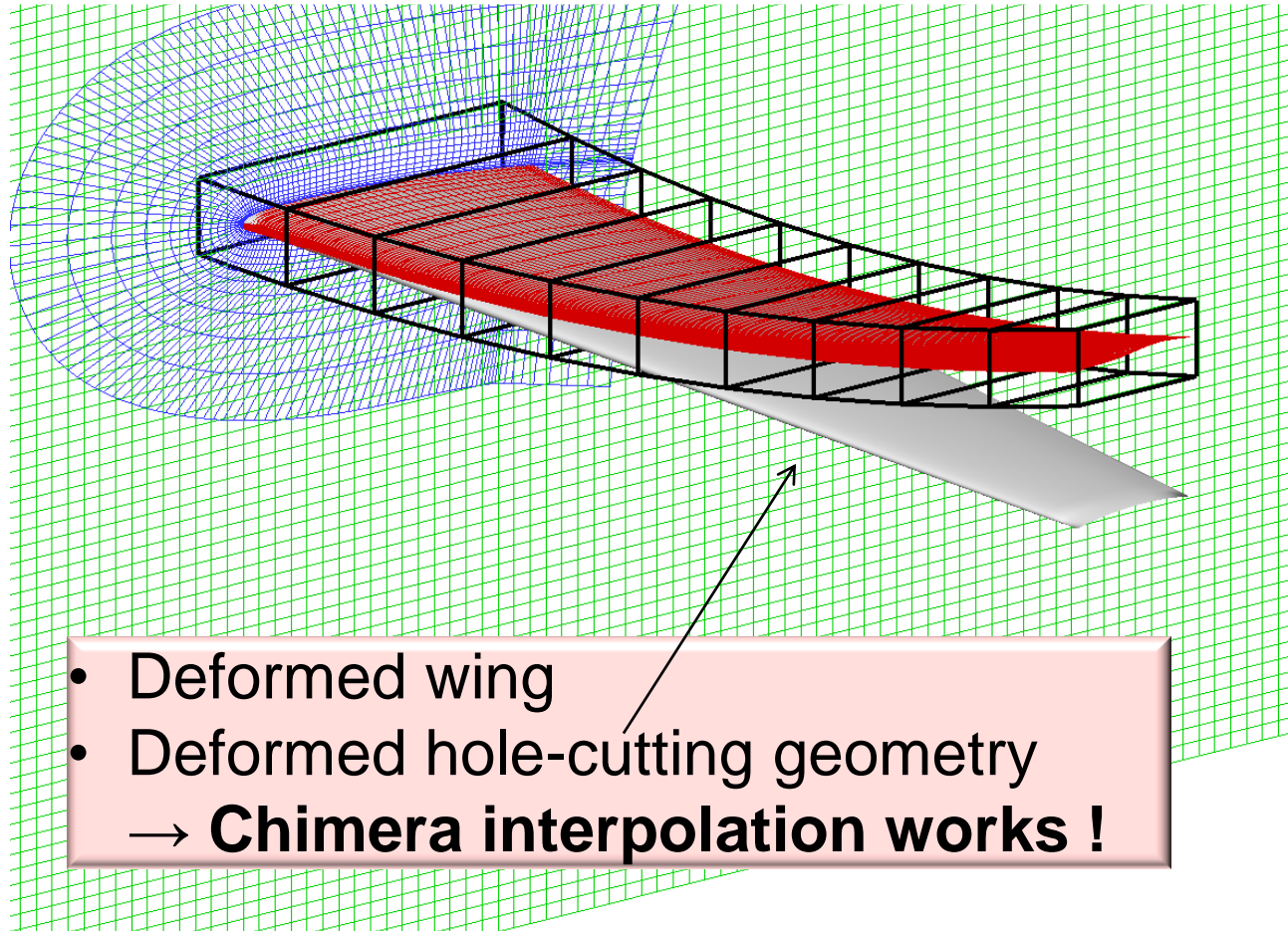


Hole-Cutting Geometries & Mesh Deformation ?

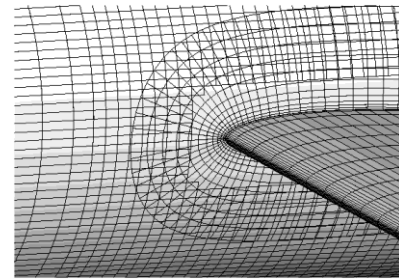


Hole-Cutting Geometries & Mesh Deformation ?

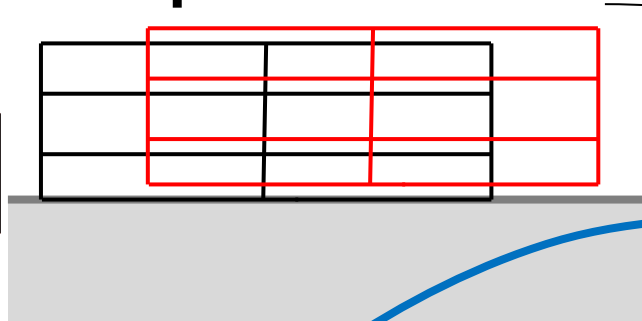
Solution: Mesh deformation operator used for overset grids is also to be applied to hole-cutting geometries



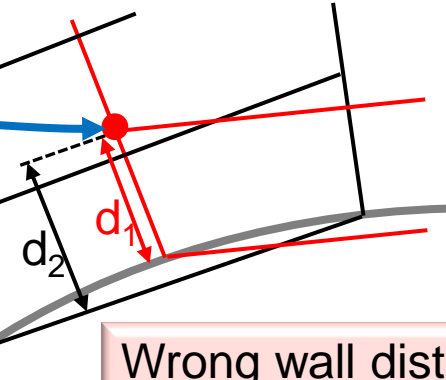
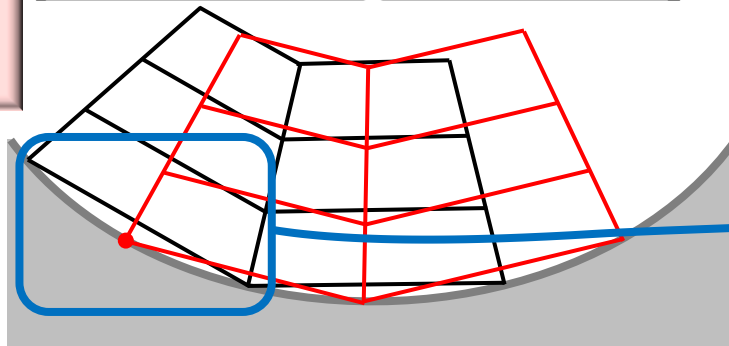
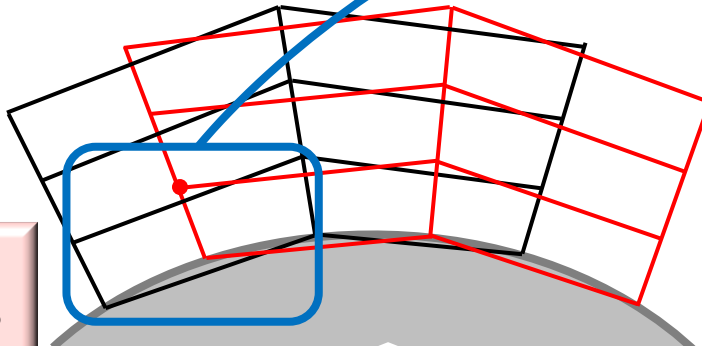
Overlapping Surface Meshes: Problem Description



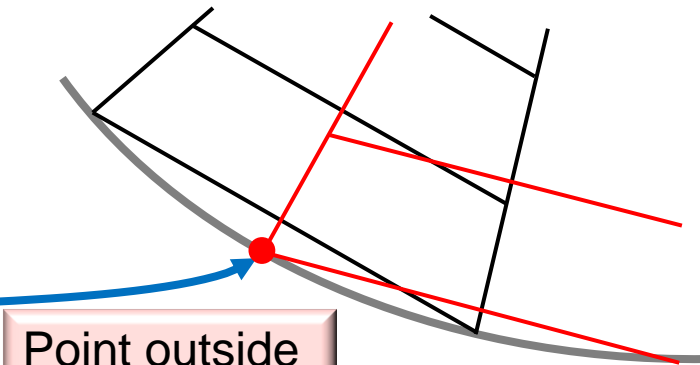
CAD
discrepancies



Different
discretizations
along curved
surfaces



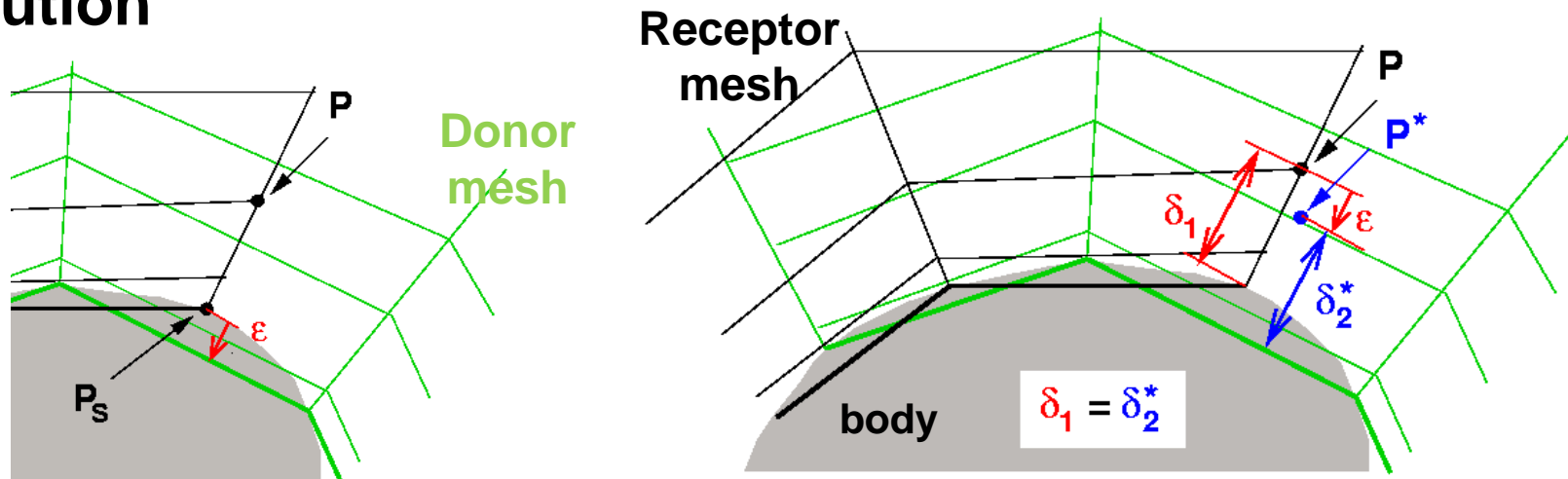
Wrong wall distance



Point outside
of donor grid



Overlapping Surface Meshes: Solution



A projection method is used, to bypass the problem:

Step 1) Project P to surface of black mesh \Rightarrow point P_s

Step 2) Project P_s in green mesh: \Rightarrow shift vector ε

Step 3) Compute virtual interpolation node P^*

$$P^* = P + w \cdot \varepsilon \quad ; \quad w = w(\delta_1) : \text{Weighting function,}$$

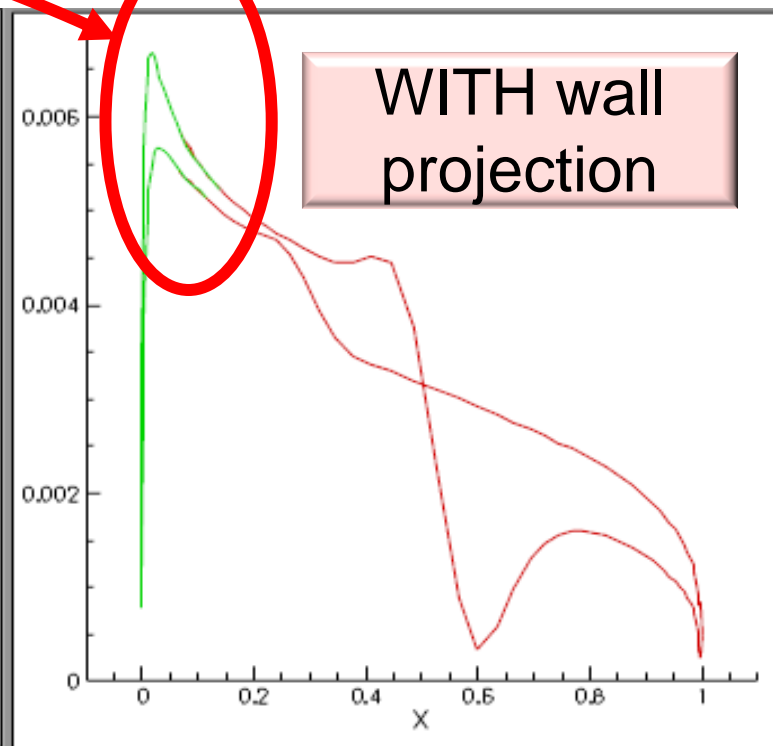
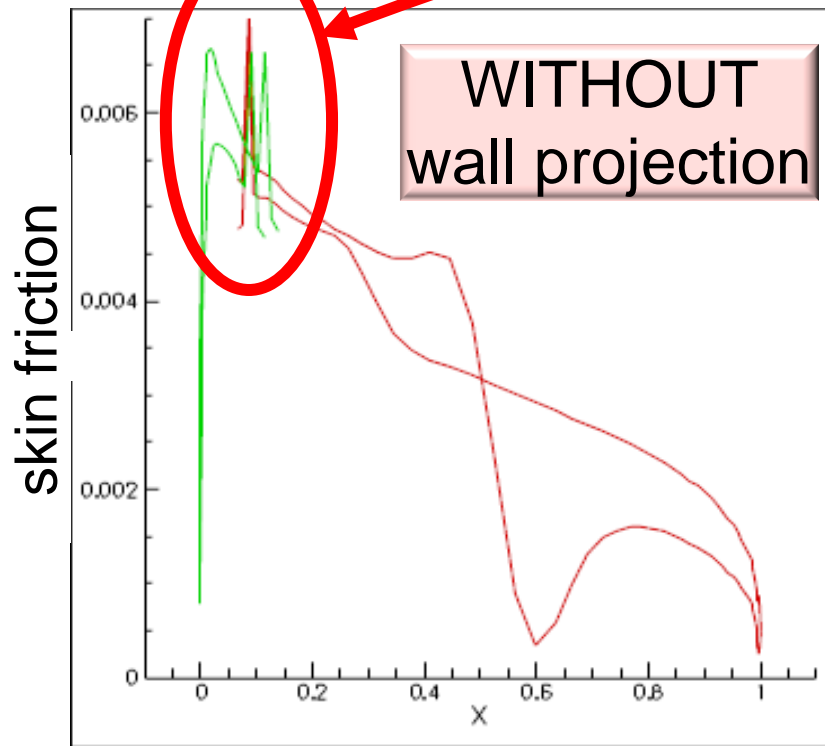
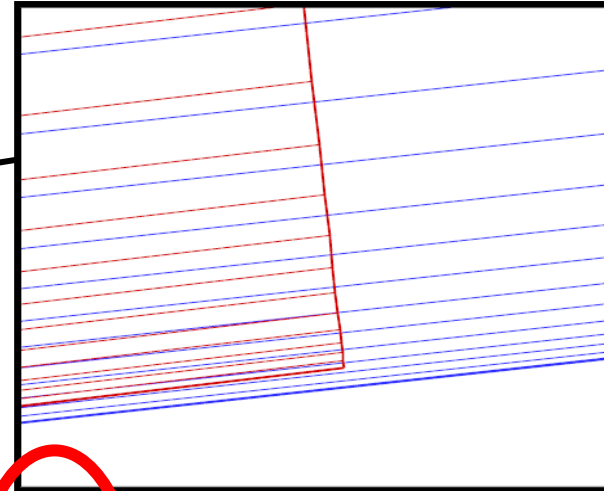
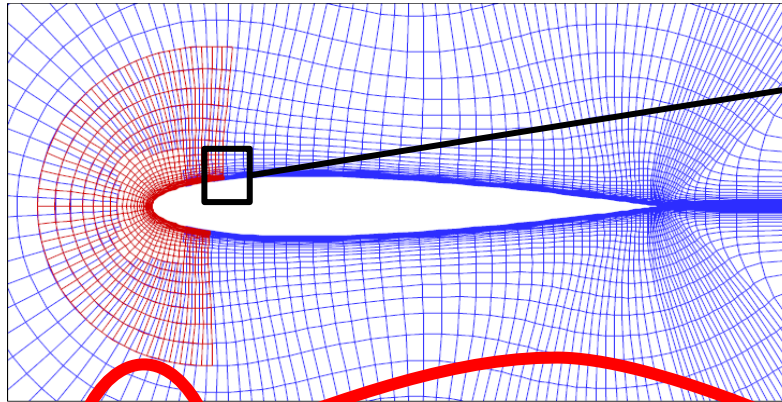
$$\delta_1 = 0 : w = 0 \quad ; \quad \delta_1 \gg 0 : w = 1$$

For interpolation nodes $P, P^* : \delta_1 = \delta_2^*$ (with $w = 1$)

Virtual interpolation node enables accurate interpolation

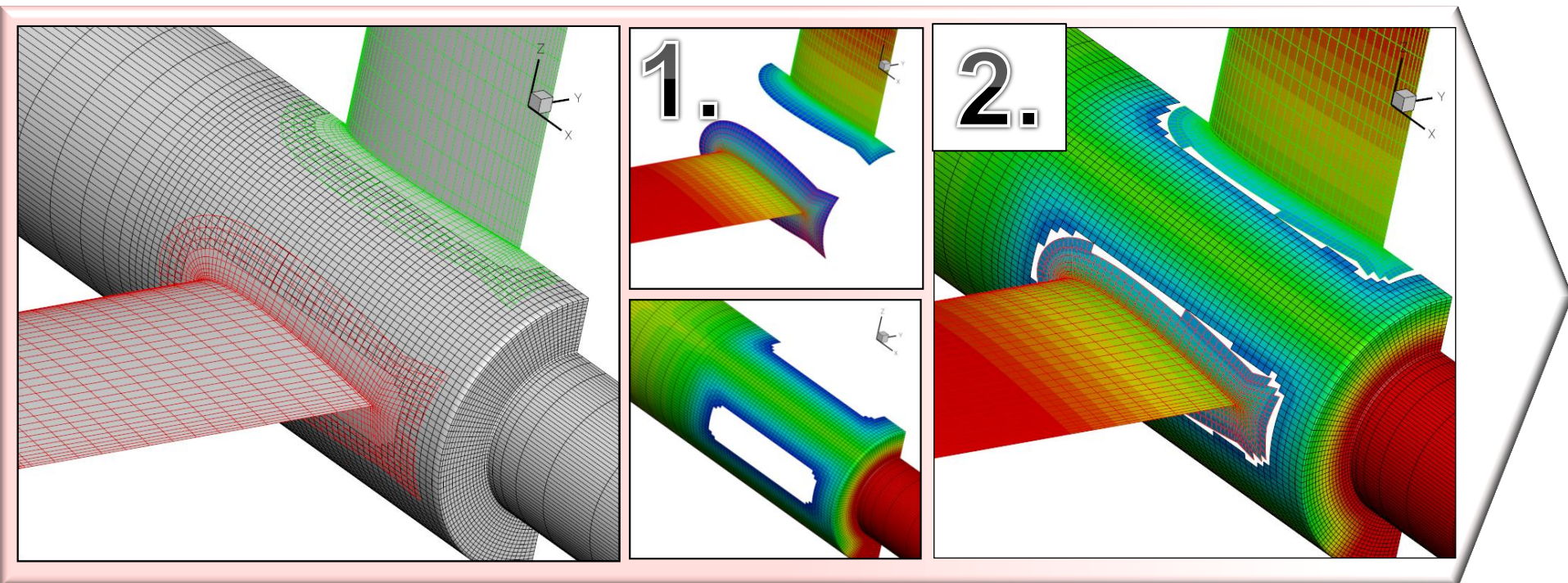


Overlapping Surface Meshes: Results w/ & w/o Chimera Wall Projection



Load Integration on Overlapping Surface Meshes

Problem: Double-counting of cells in regions with overlapping surface grids
=> wrong integral loads



Task: Create an air-tight surface grid , i.e. remove overlap and fill resulting gaps by triangulation – **zipper grids**

Step 1) Mark cells by distance to Chimera interpolation layer

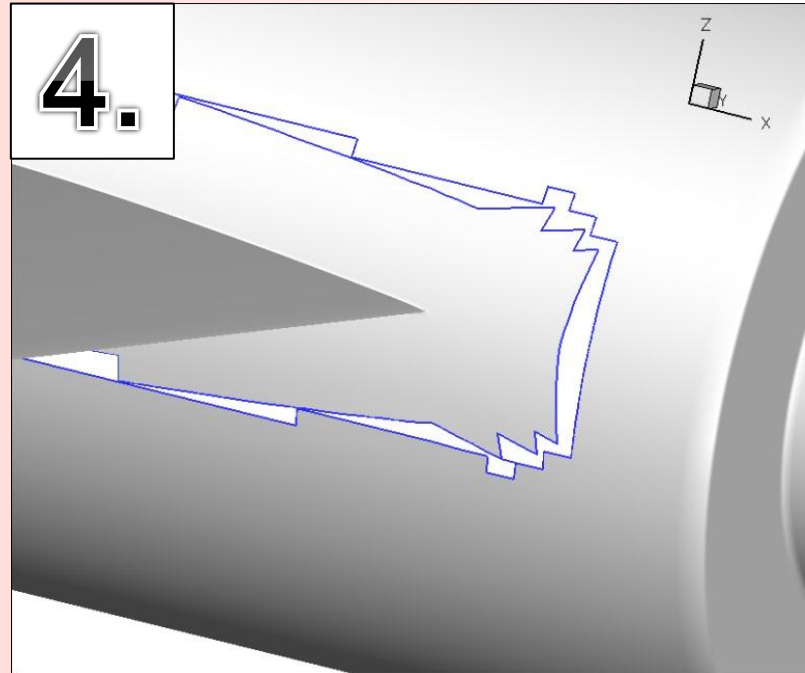
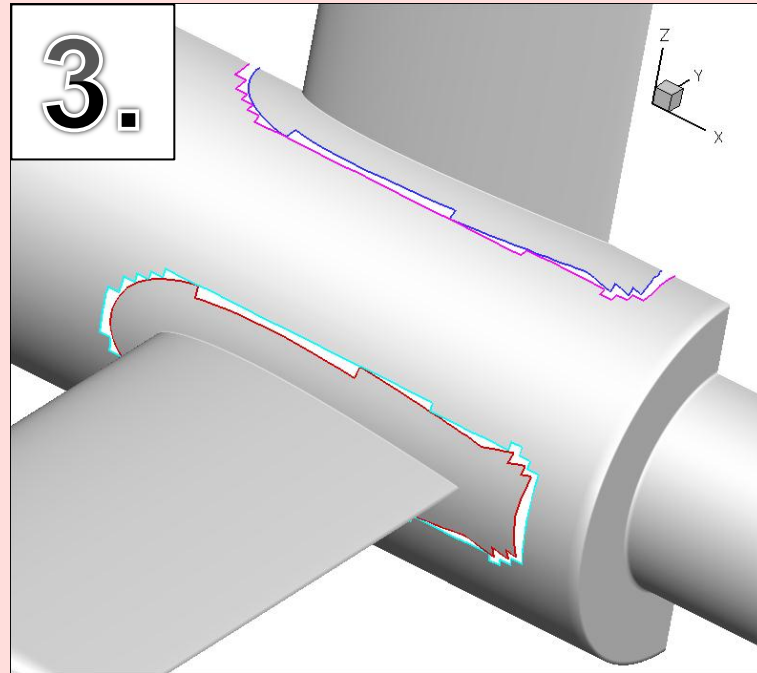
Step 2) Remove overlapping cells with low priority

=> Overlapping removed , gap has same distance to both interpolation layers



Load Integration on Overlapping Surface Meshes

Problem: Double-counting of cells in regions with overlapping surface grids
=> wrong integral loads



Task: Create a air-tight surface grid = Remove overlap and fill gaps by triangulation – **zipper grids**

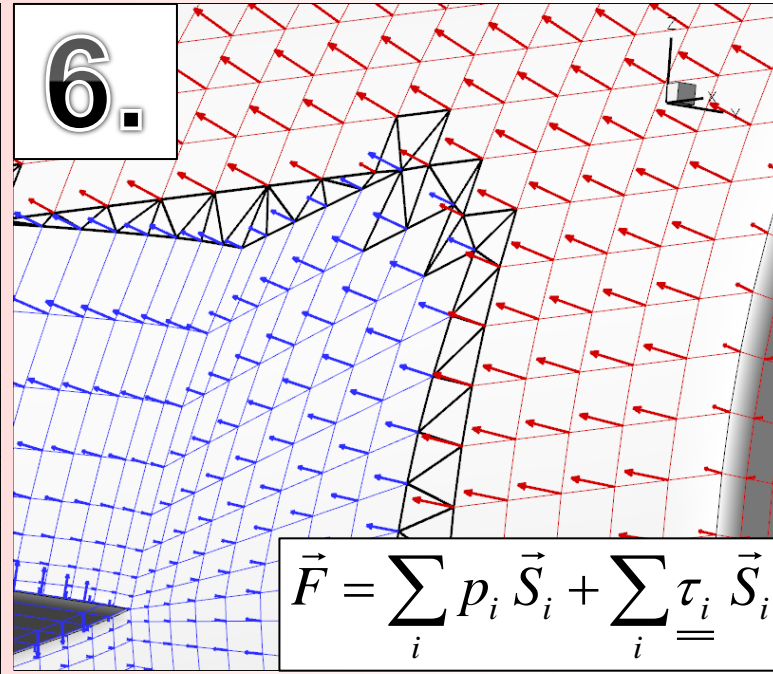
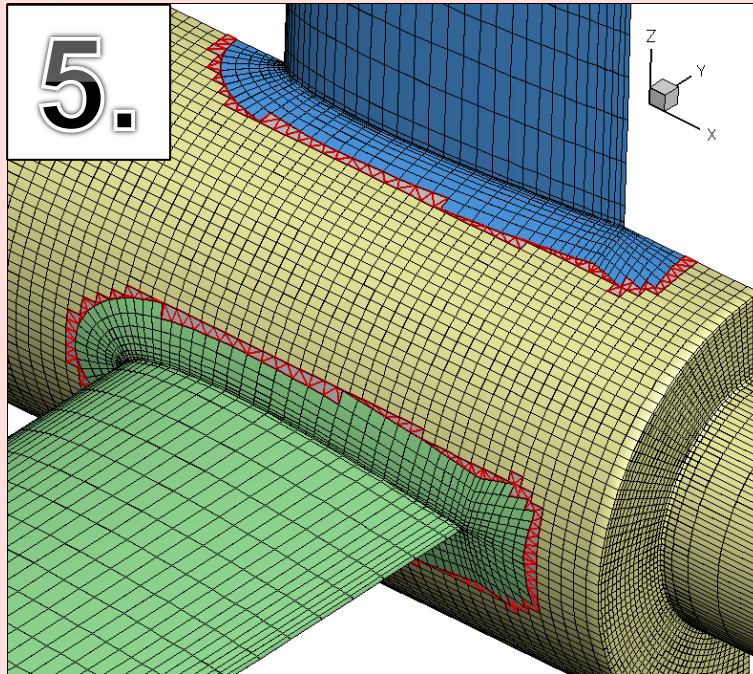
Step 3) Extract border lines of resulting grids

Step 4) Gather opposing border lines to build gap data that is to be triangulated



Load Integration on Overlapping Surface Meshes

Problem: Double-counting of cells in regions with overlapping surface grids
=> wrong integral loads



$$\vec{F} = \sum_i p_i \vec{S}_i + \sum_i \tau_i \vec{S}_i$$

Task: Create a air-tight surface grid = Remove overlap and fill gaps by triangulation – **zipper grids**

Step 5) Delaunay triangulation

Step 6) Force summation on non-overlapping grid

In the past: Only available as sequential postproc. tool

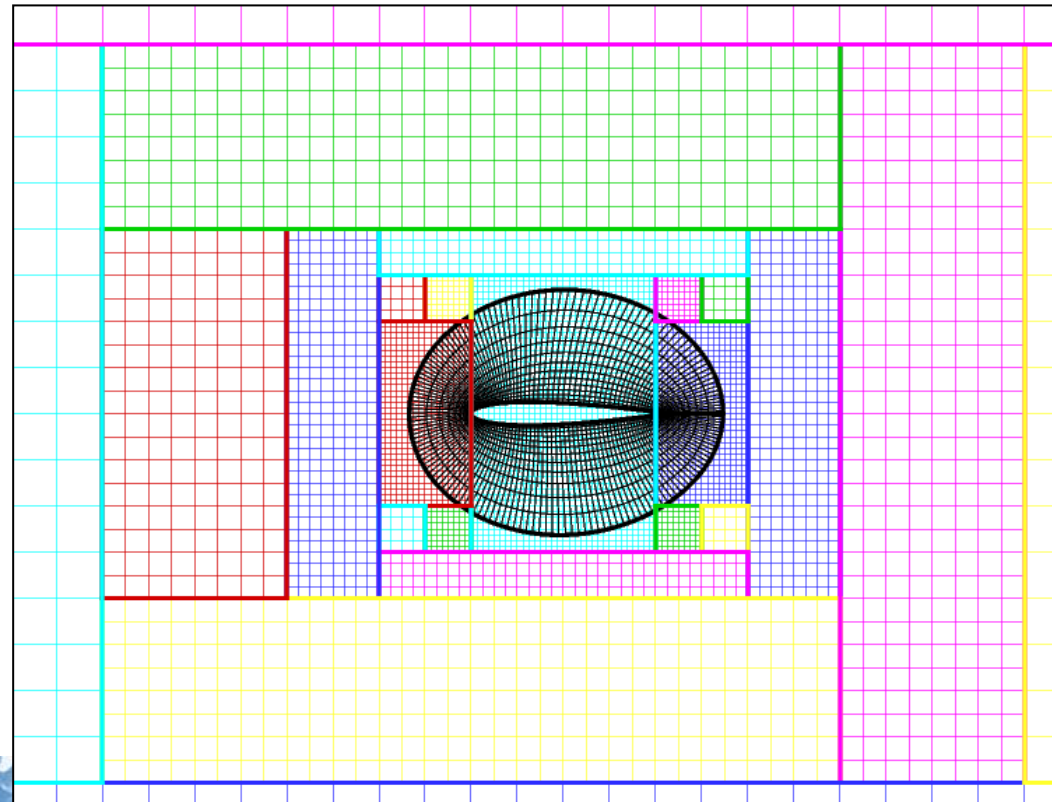
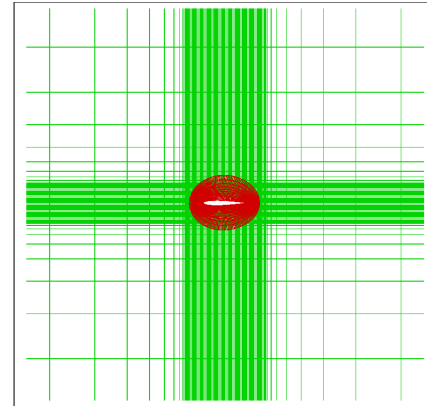
Now: Parallel version directly integrated into TAU



Cartesian Background Grid Generator

Problem: Manual generation of background grid with sufficient overlap & resolution cumbersome and time-consuming

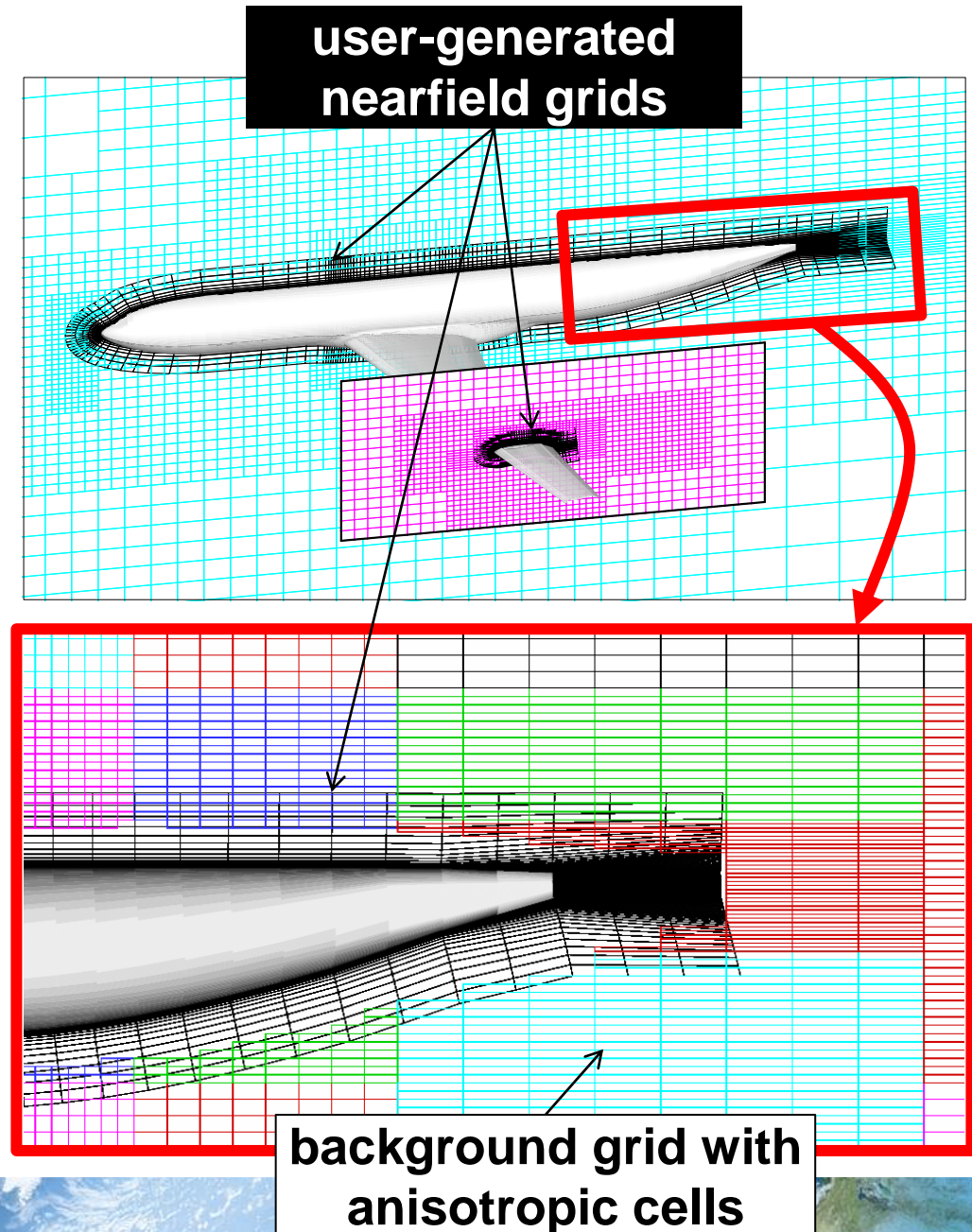
Idea: Automatic generation of Cartesian multiblock grids with hanging nodes (only FLOWer; TAU does not feature hanging nodes capability yet)



Cartesian Background Grid Generator

Features:

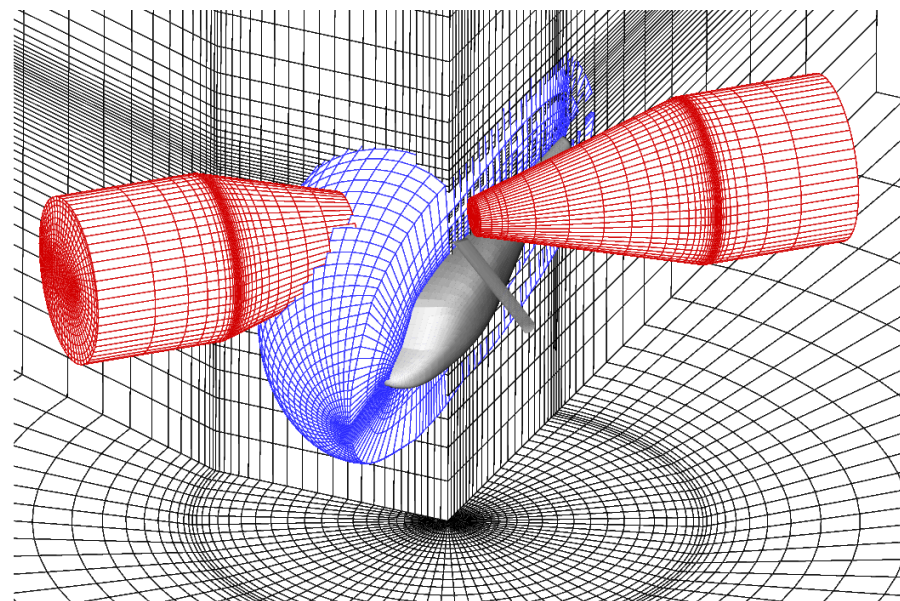
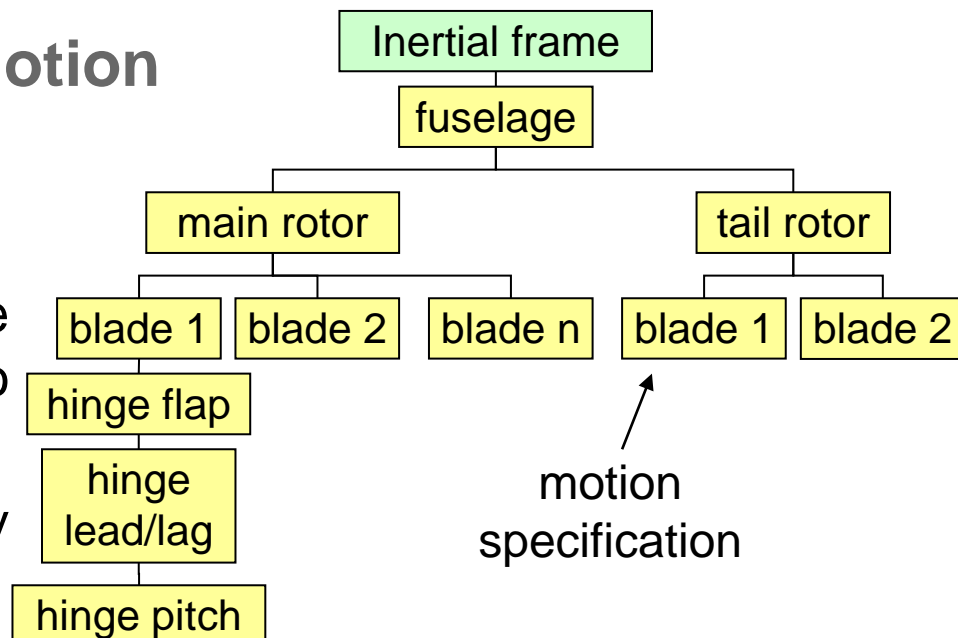
- Very coarse initial background grids (8x8x8 cells) are adapted consecutively to the nearfield grid's cell sizes
- Anisotropic refinements possible
=> Reduction of interpolation errors
=> Prevents from insufficient cell overlap
- Minimisation of the number of blocks by automatic concatenation



Overset Grids in Relative Motion

Specification of rigid body motions

- Tree-like data structure (=hierarchy) is used to prescribe grid motion
- Any grid can be linked to any motion specification
- TAU code: grid motion can be set conveniently (required for 6DoF app.) using TAU's Python interfaces



Applications



Coupled CFD-6DoF Simulation of Airdrop Scenario

MiTraPor Test Case

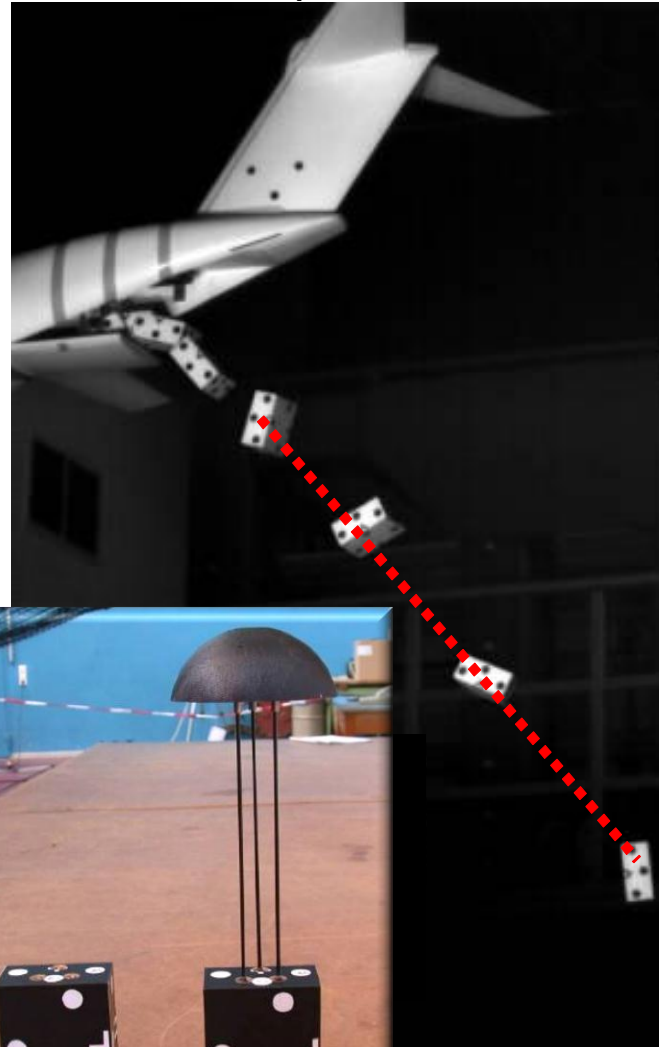
Example airdrop:



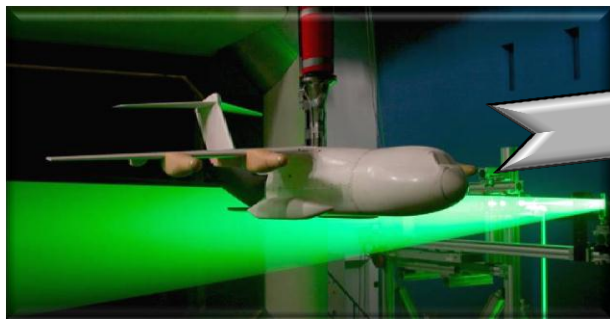
<http://www.youtube.com/watch?v=eQwJnVad5L4>

- Measurement of location of generic boxes w/ and w/o parachute
- Flow conditions:
 $v_{\text{inf}} = 18\text{m/s}$, $\alpha = 6^\circ$, $\text{Re} = 4 \times 10^5$

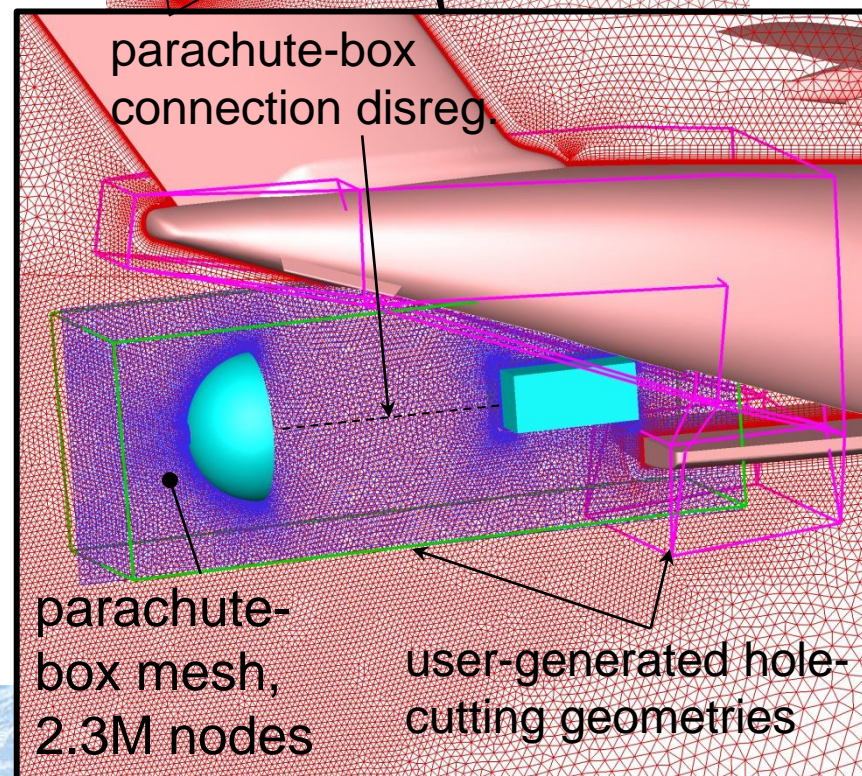
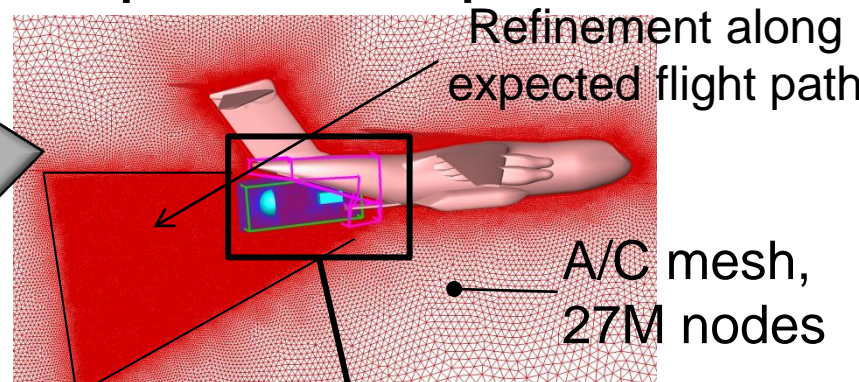
MiTraPor airdrop:



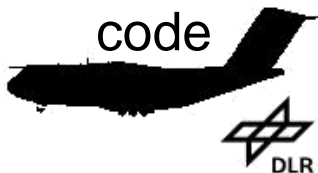
Coupled CFD-6DoF Simulation of Airdrop Scenario MiTraPor Test Case



Computational setup:

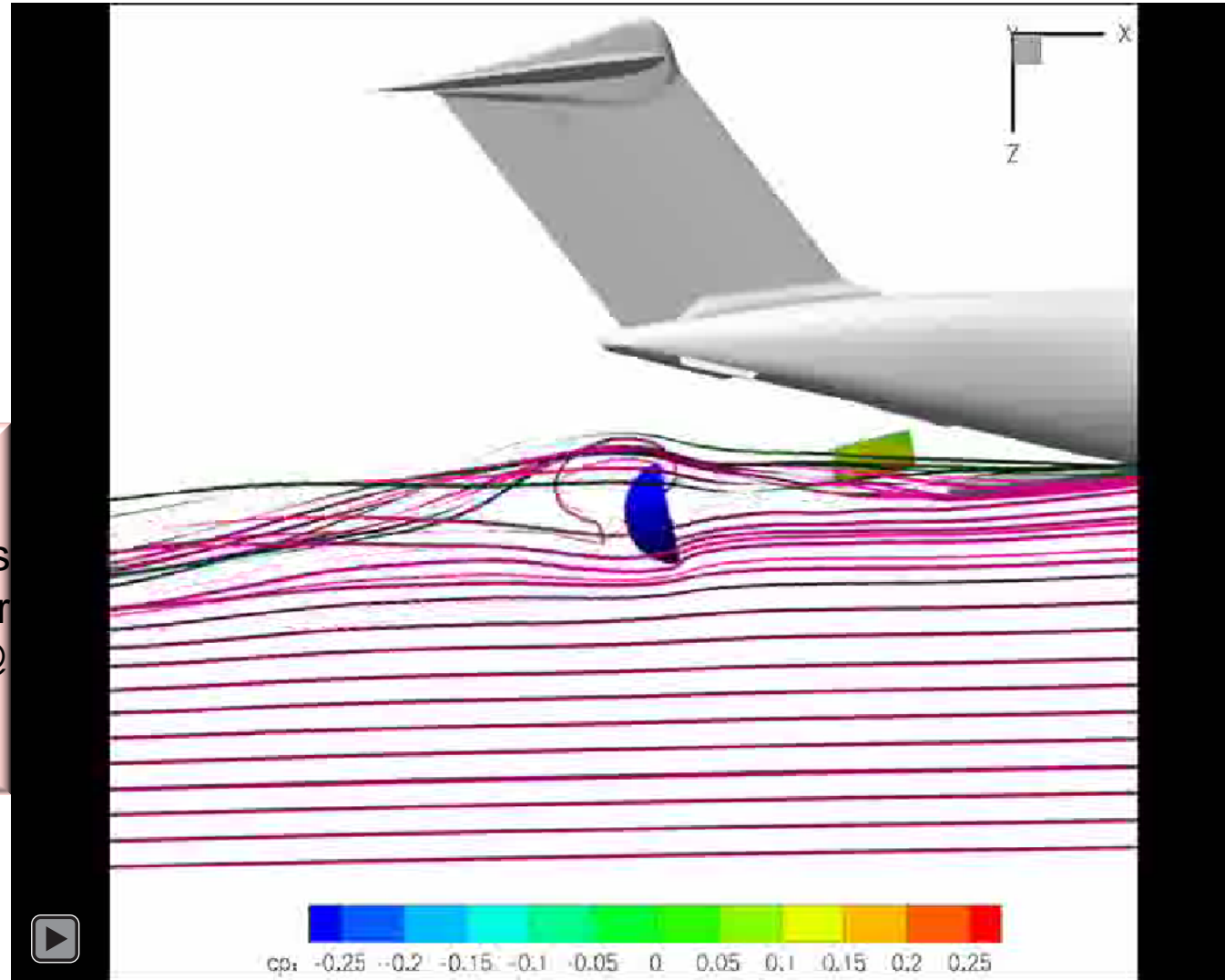


- Making use of overset grid technique with semi-automatic hole cutting
 - Unstruct. background A/C mesh
 - Unstruct. mesh around parachute-box config.
- Tight coupling of TAU to 6DoF code

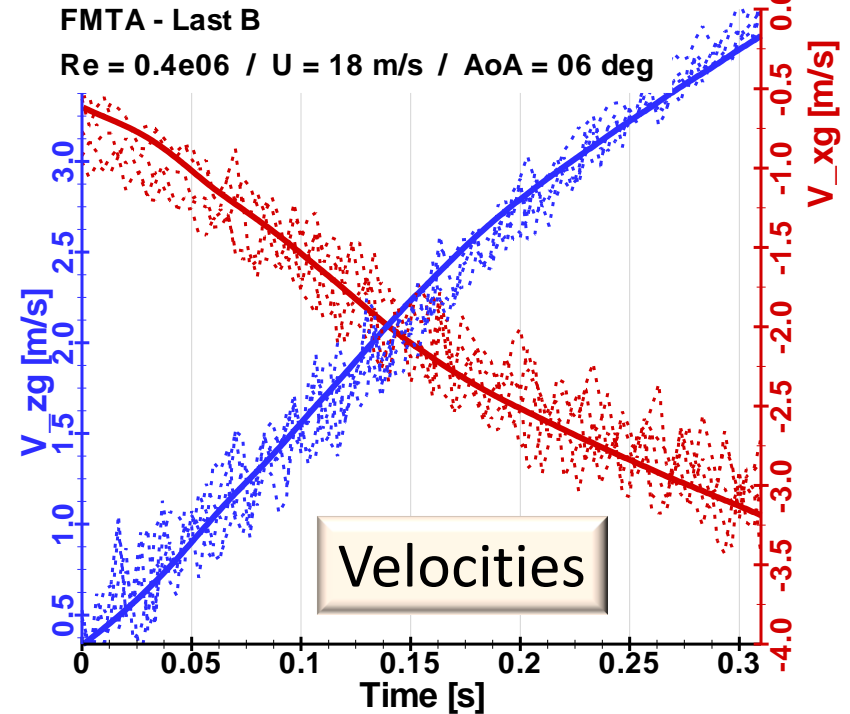
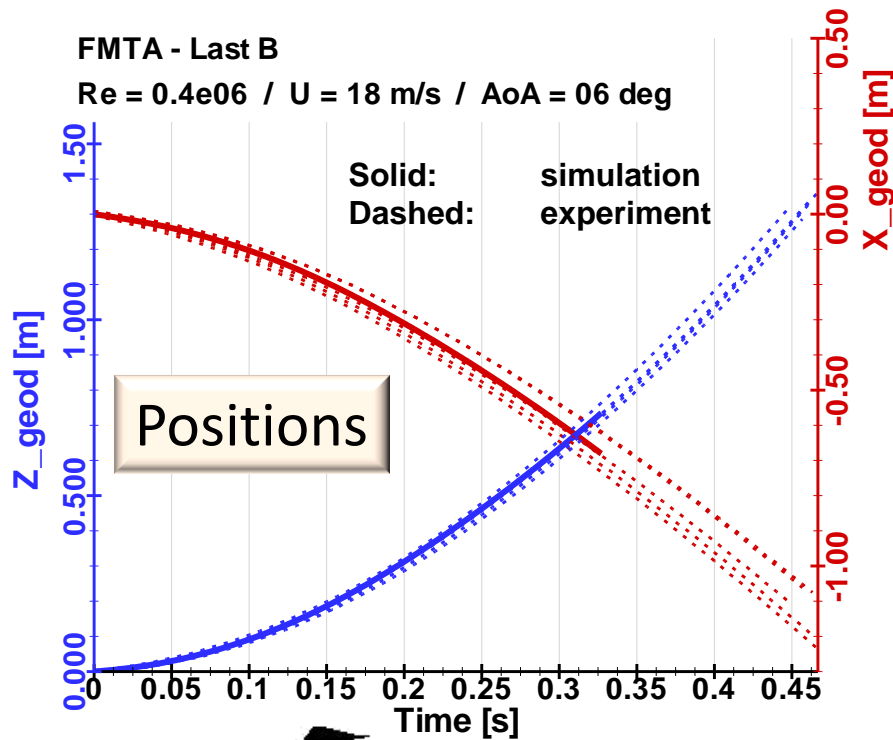
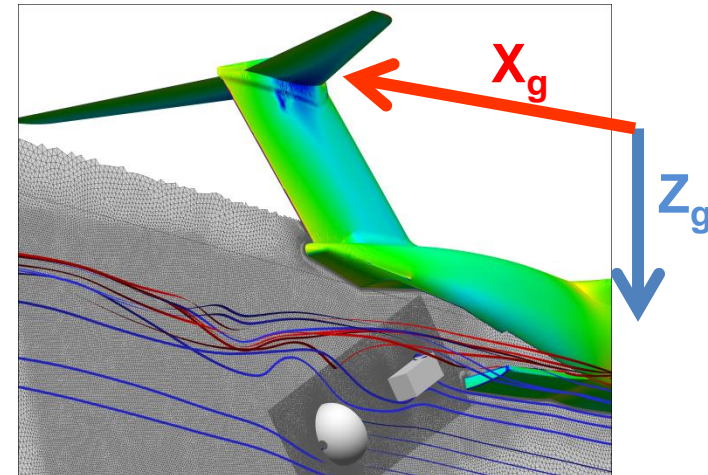


Coupled CFD-6DoF Sim. of Airdrop Scenario

Computing time:
42.6M pts., 144 procs:
160h (~7d) for 0.33s
real time, 53min per
phys. time step @
600Hz resol.

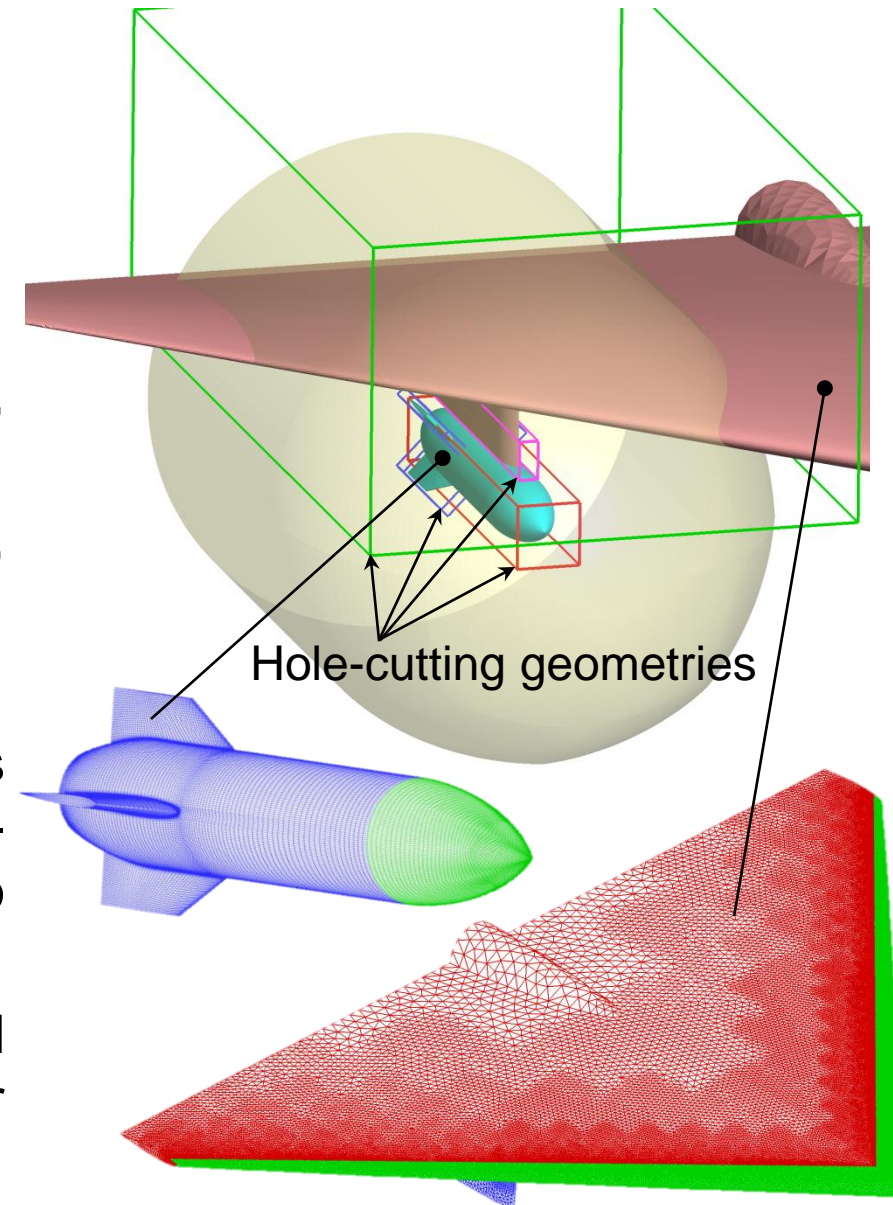


Coupled CFD-6DoF Simulation of Airdrop Scenario: MiTraPor Test Case – Comparison of Computed & Measured Trajectories



Coupled CFD-6DoF Sim. of Store Release AFRL* Test Case

- Activity within GARTEUR SIG 47
- Flow conditions: $Ma = 0.95$, $\alpha = 0.0^\circ$, $Re = 4.1m$
- Experiment conducted by AFRL, see RTO-TR-26, ch. 23
- Meshes:
 - **Store:** Structured Ansys ICEM-CFD HEXA Navier-Stokes mesh converted to TAU format, 3.1M nodes
 - **Delta wing:** Unstructured CentaurSoft Centaur Euler mesh, 600k nodes



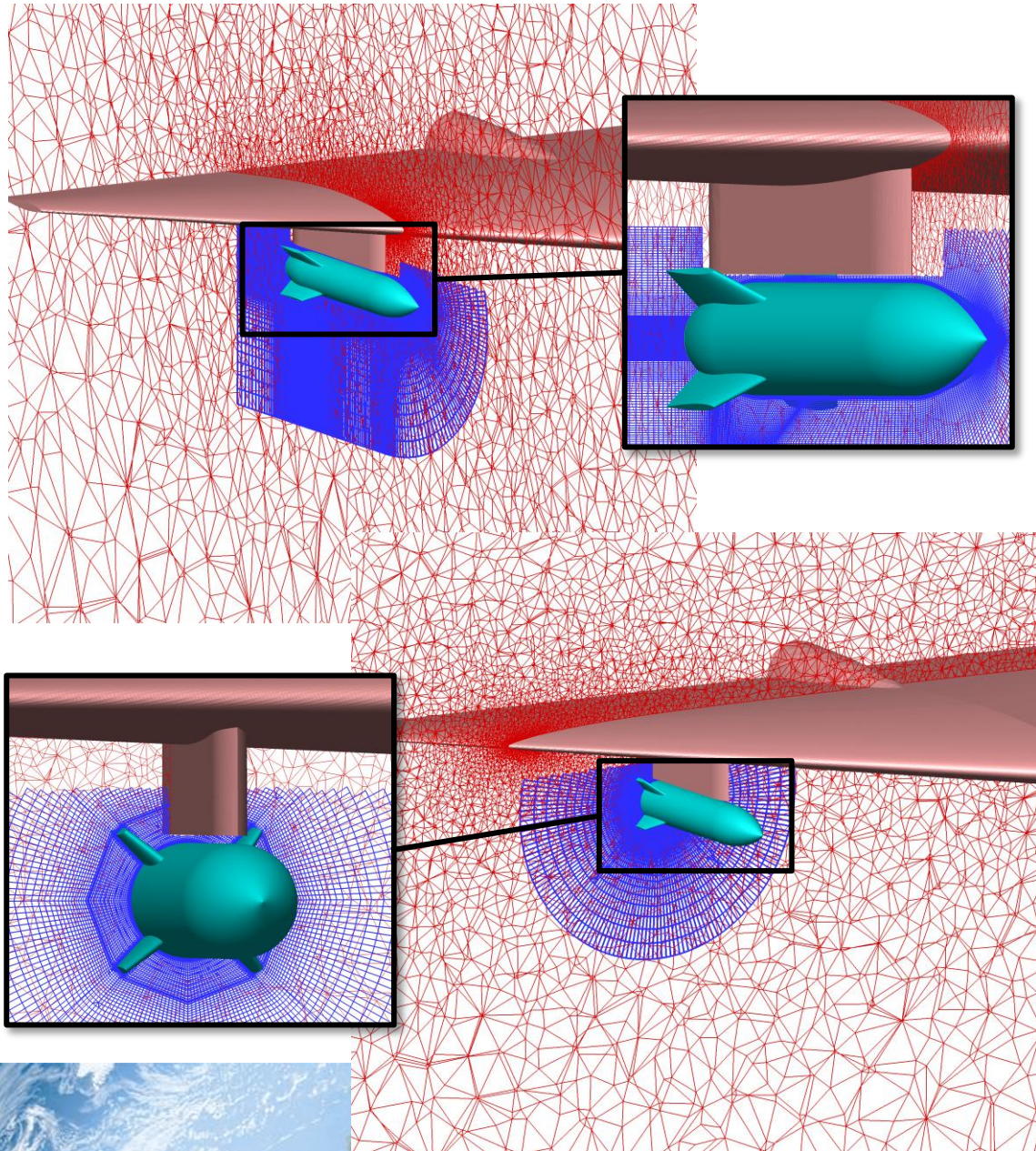
* Air Force Research Laboratory, Wright-Patterson Air Force Base



Coupled CFD-6DoF Sim. of Store Release AFRL Test Case

Difficulty:

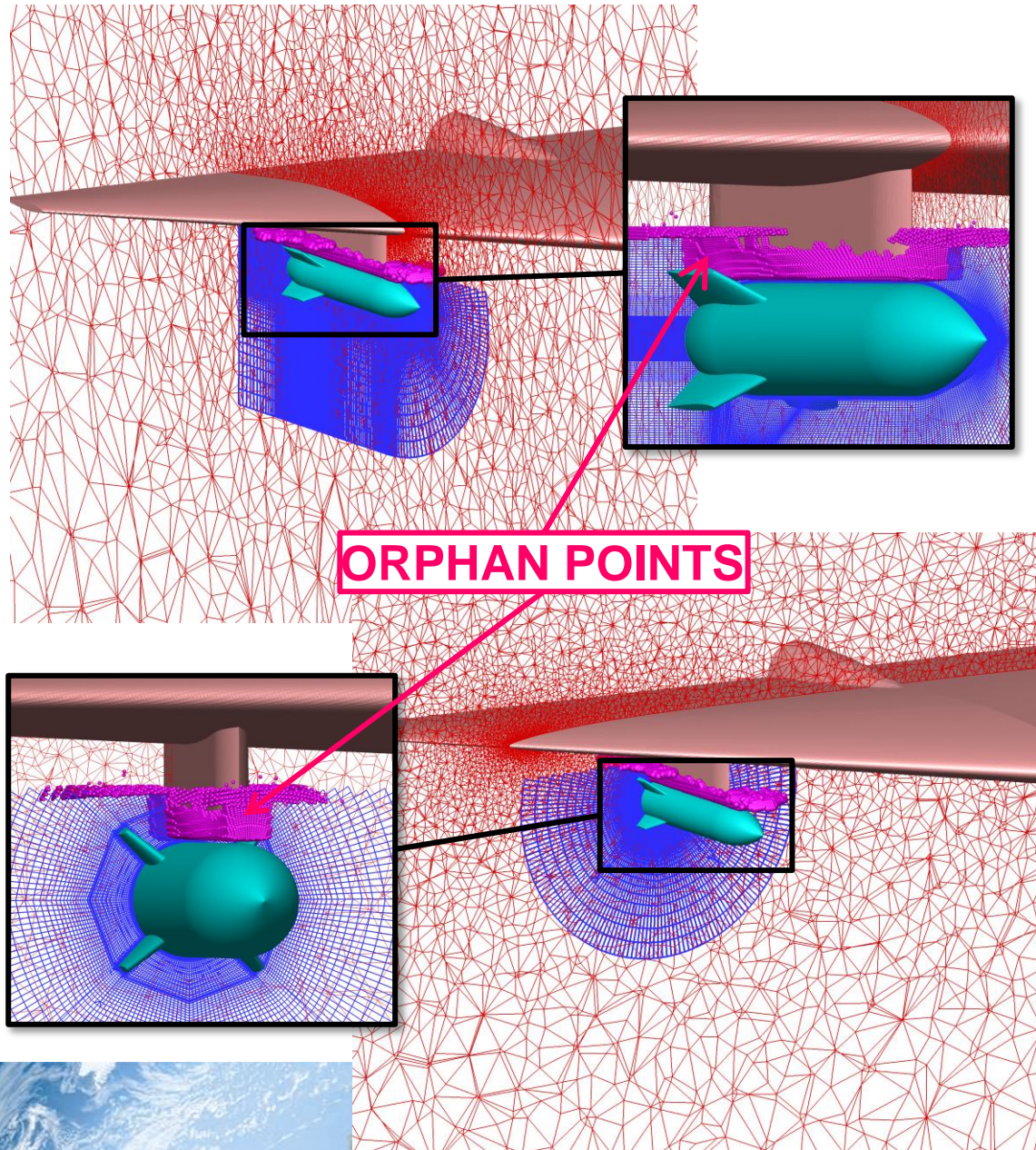
At $t=0$ store & pylon are
very close



Coupled CFD-6DoF Sim. of Store Release AFRL Test Case

Difficulty:

At $t=0$ store & pylon are very close => With the original mesh, not all donor cells could be found



Coupled CFD-6DoF Sim. of Store Release AFRL Test Case

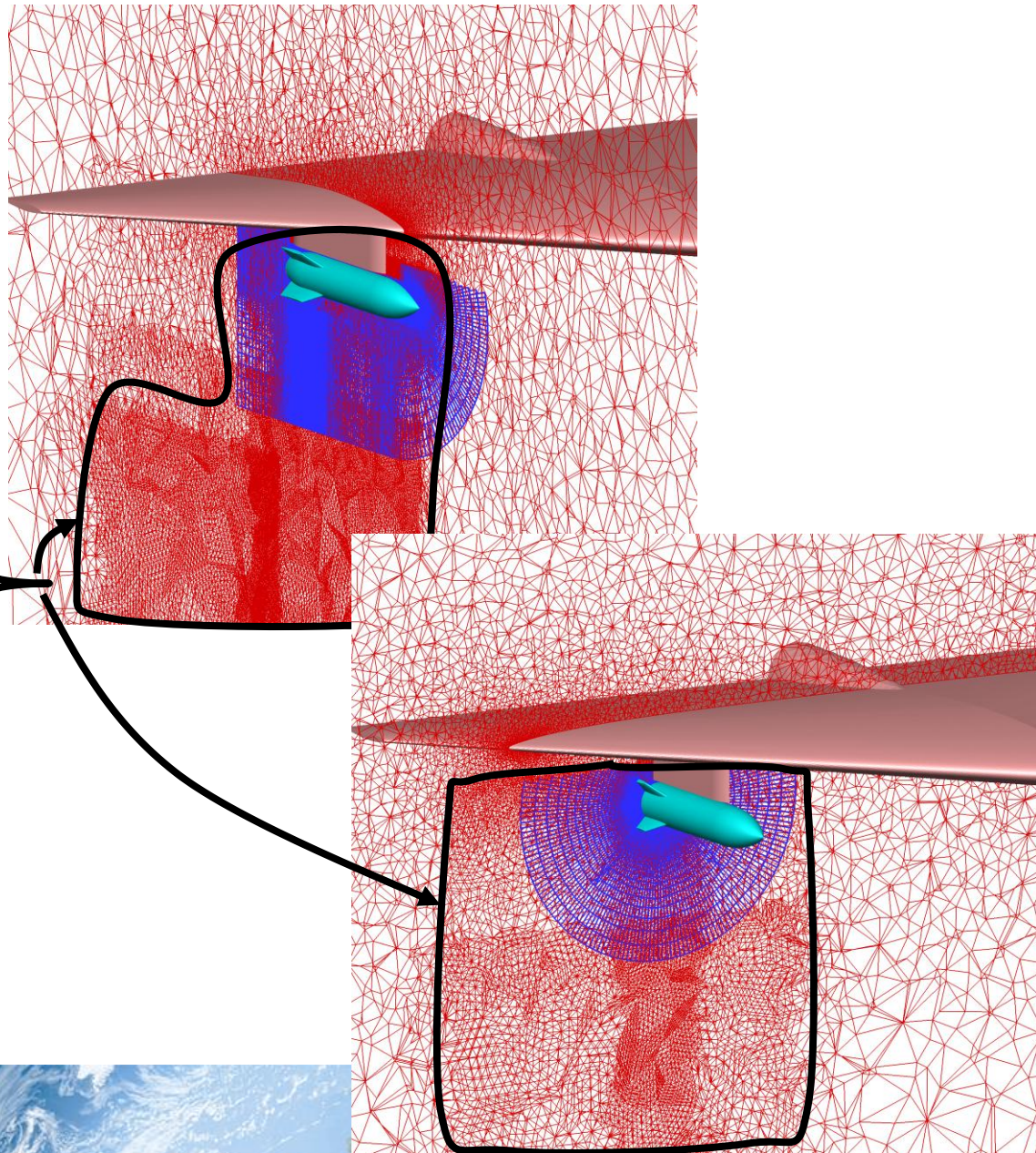
Difficulty:

At $t=0$ store & pylon are very close => With the original mesh, not all donor cells could be found

Approach for solving the problem:

Uniform adaptation of the delta wing mesh

- ... close to the pylon
- ... in expected flight path area



Coupled CFD-6DoF Sim. of Store Release

AFRL Test Case

Difficulty:

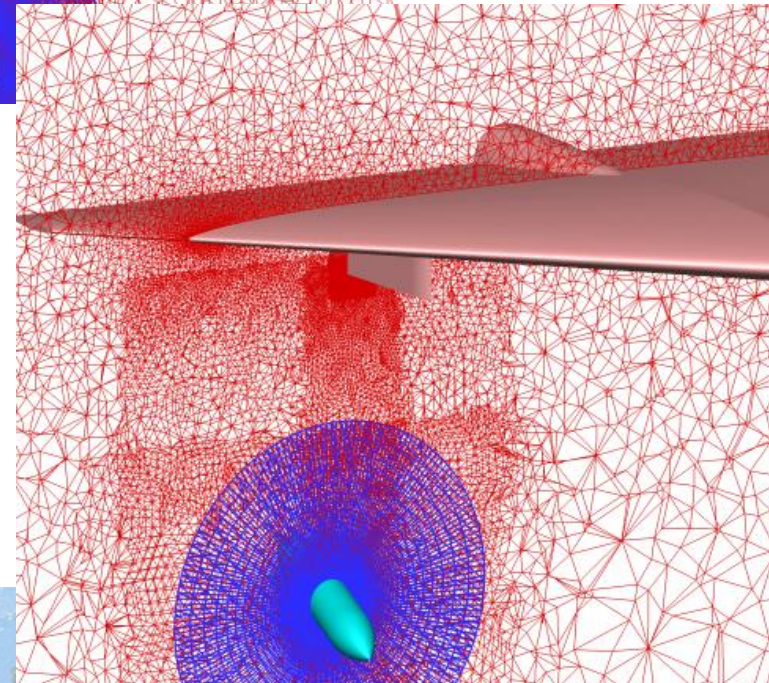
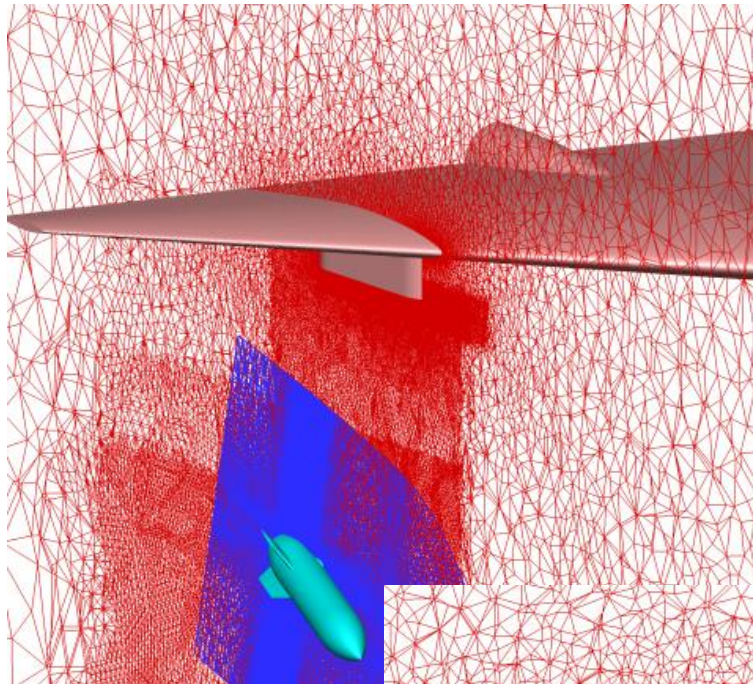
At $t=0$ store & pylon are very close => With the original mesh, not all donor cells could be found

Approach for solving the problem:

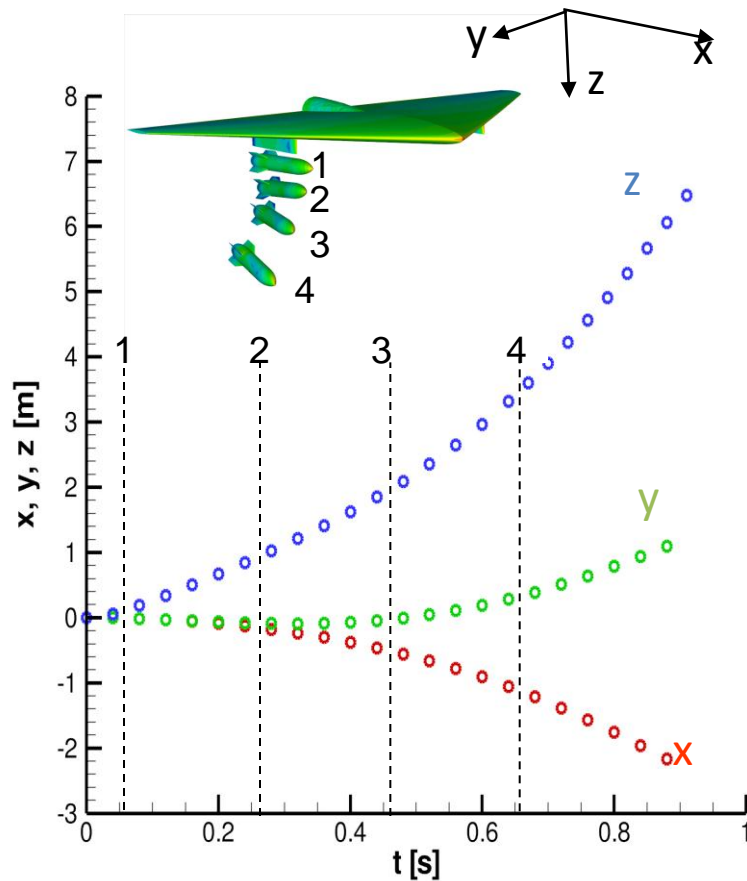
Uniform adaptation of the delta wing mesh

- ... close to the pylon
- ... in expected flight path area

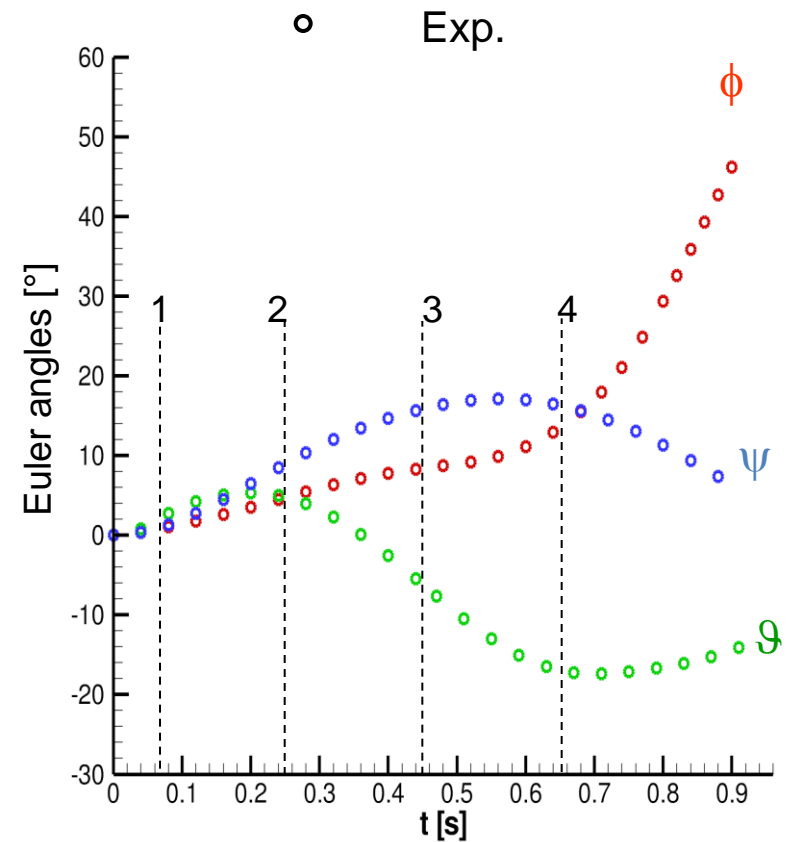
⇒ With adaptation approach the simulation worked



Coupled CFD-6DoF Simulation of Store Release AFRL Test Case



Locations



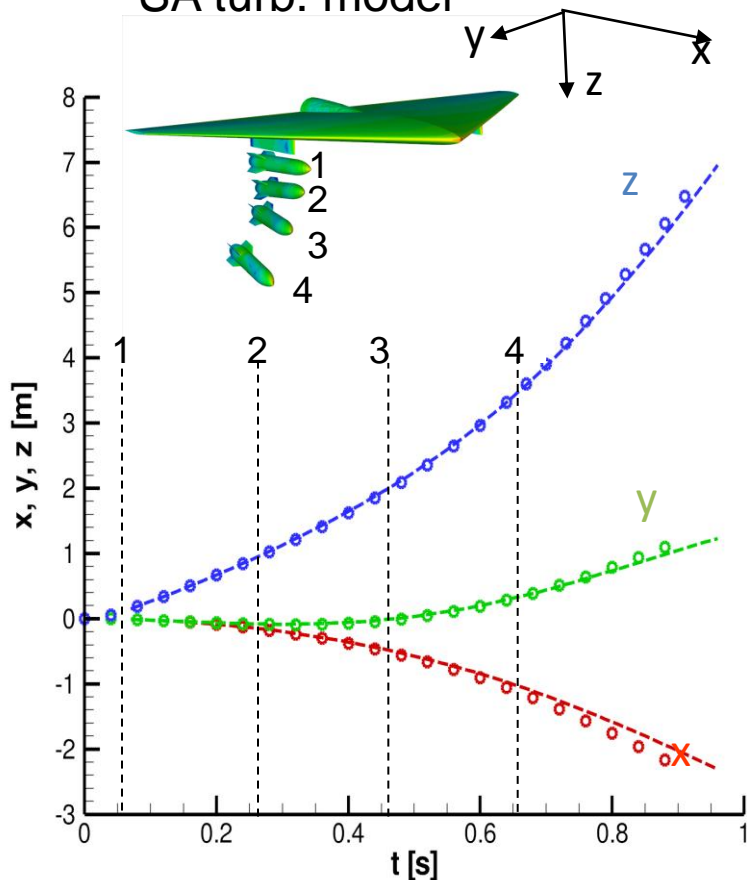
Rotations

Coupled CFD-6DoF Simulation of Store Release

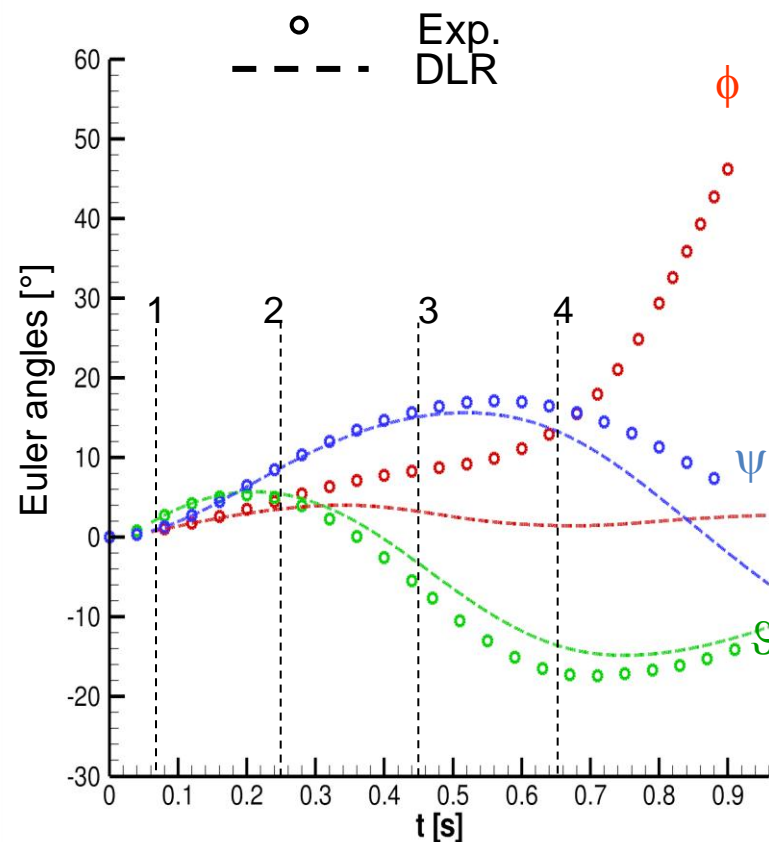
AFRL Test Case

DLR's simulation:

- Strong coupling of CFD-6DoF (unsteady)
- SA turb. model



Locations



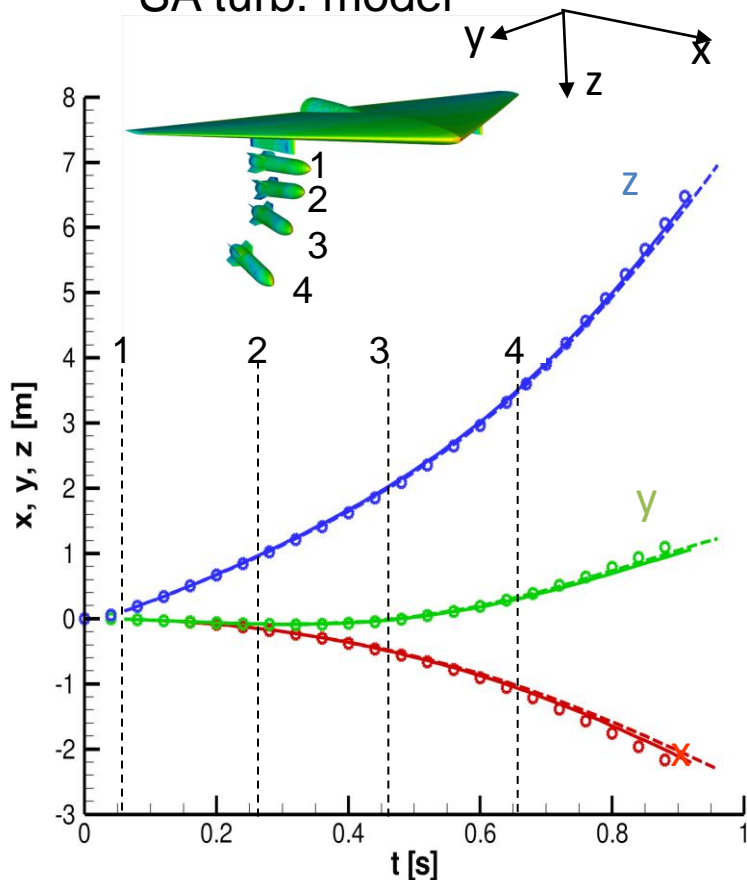
Rotations

Coupled CFD-6DoF Simulation of Store Release

AFRL Test Case

DLR's simulation:

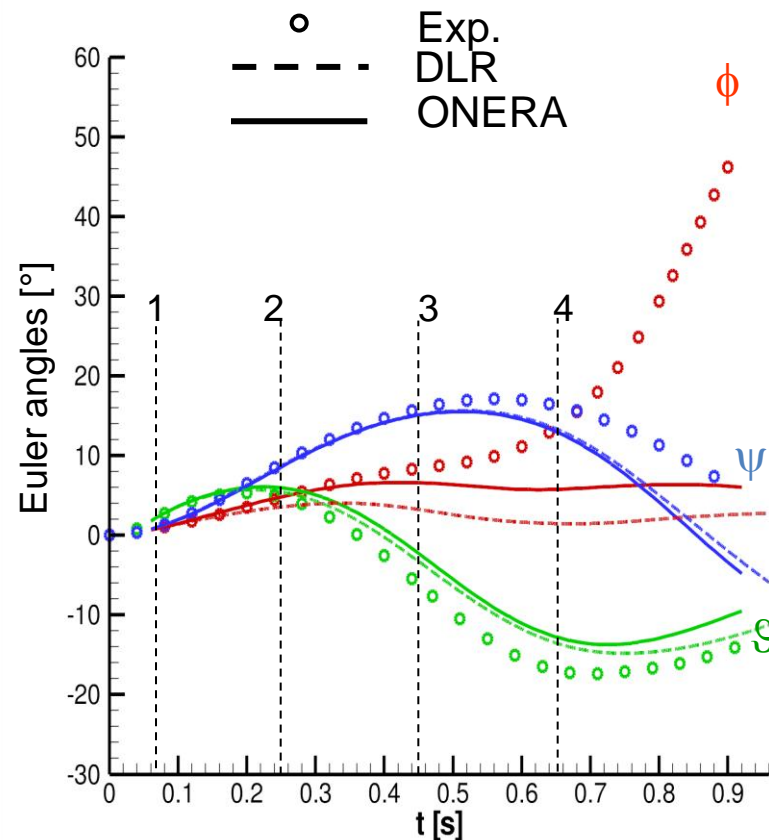
- Strong CFD-6DoF coupling (unsteady)
- SA turb. model



Locations

ONERA's simulation:

- Quasi-steady coupling CFD-6DoF
- SA turb. model

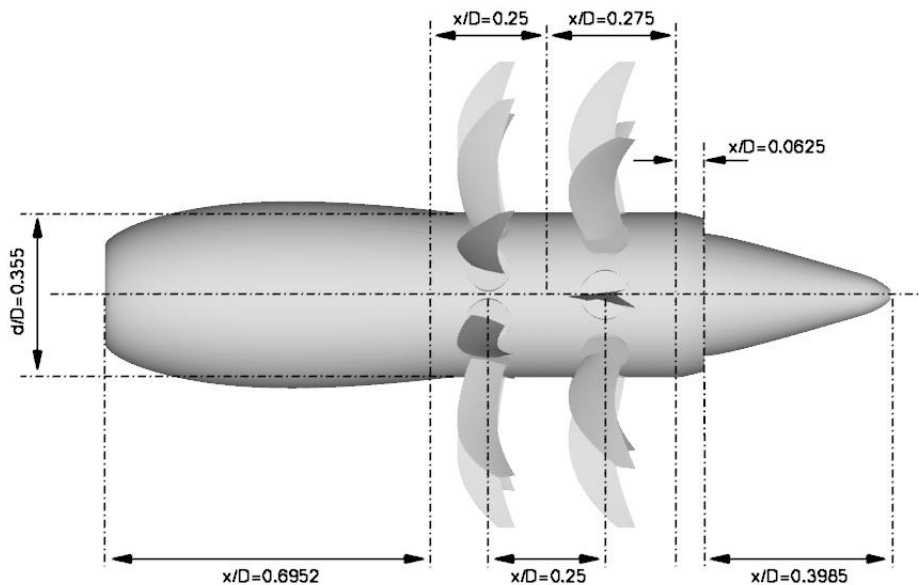
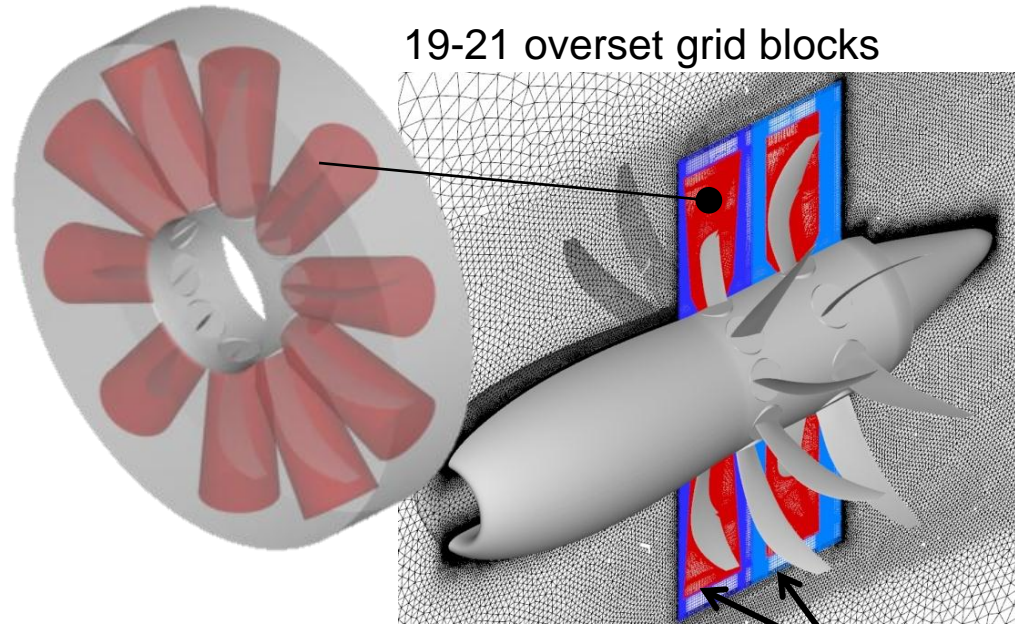


Rotations

Open Rotor Applications: CROR Flow Analysis

Here: Isolated rotor case

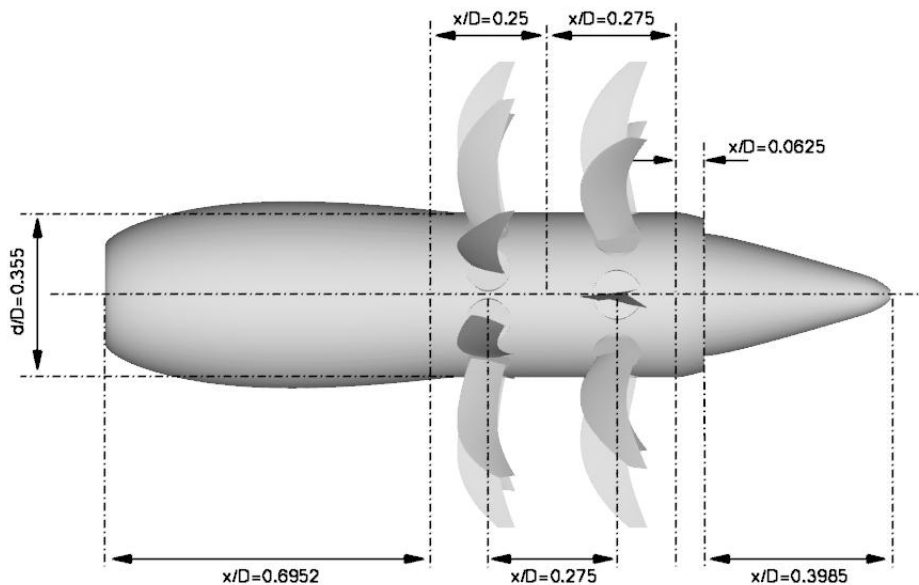
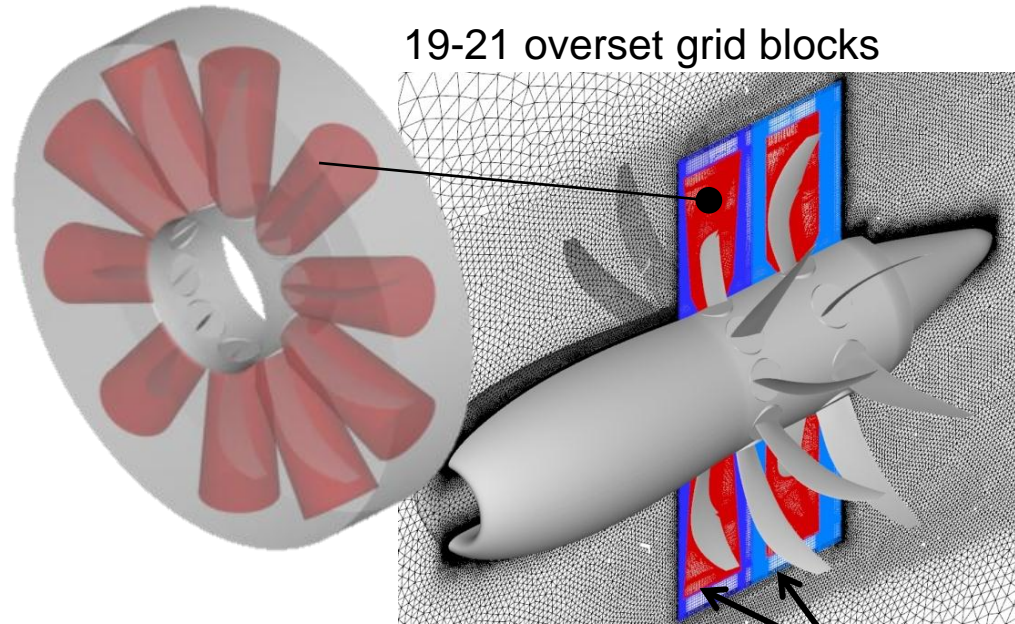
- Unstruct. background grid, struct. spinner & blade grids, „pre-generated“ holes used



Open Rotor Applications: CROR Flow Analysis

Here: Isolated rotor case

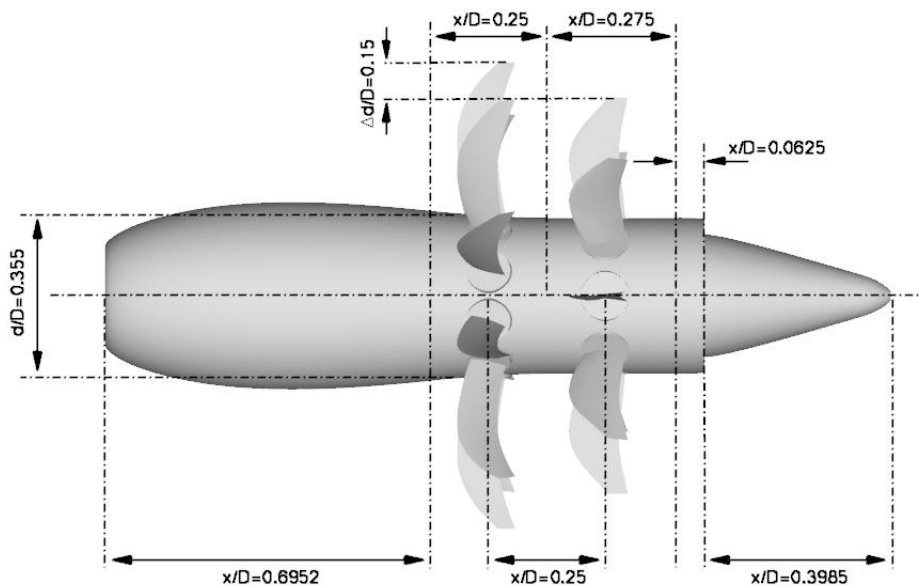
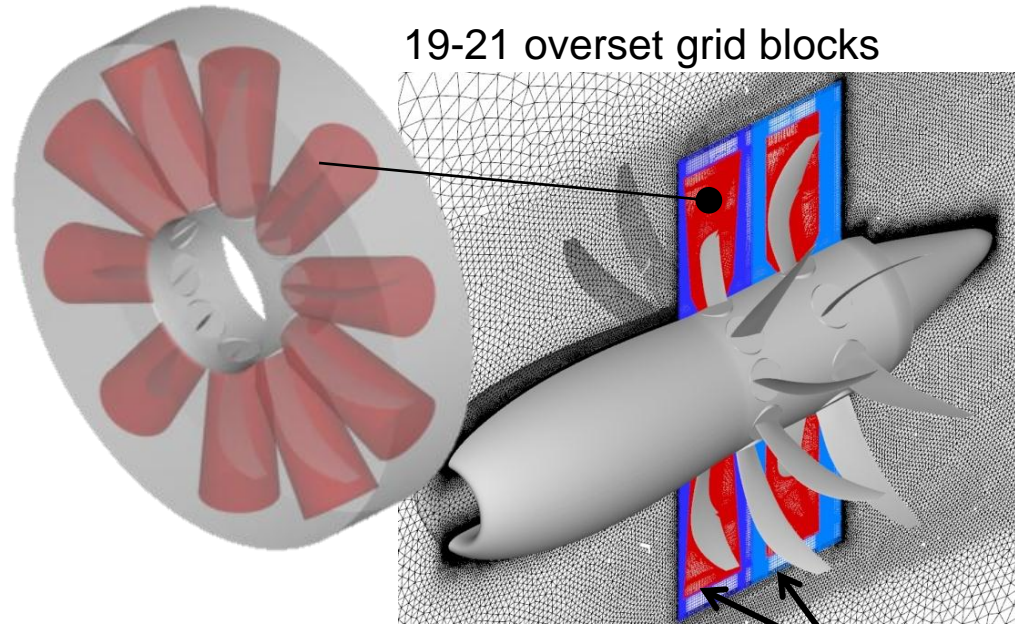
- Unstruct. background grid, struct. spinner & blade grids, „pre-generated“ holes used
- Perform. & noise analysis of many config. variations



Open Rotor Applications: CROR Flow Analysis

Here: Isolated rotor case

- Unstruct. background grid, struct. spinner & blade grids, „pre-generated“ holes used
- Perform. & noise analysis of many config. variations

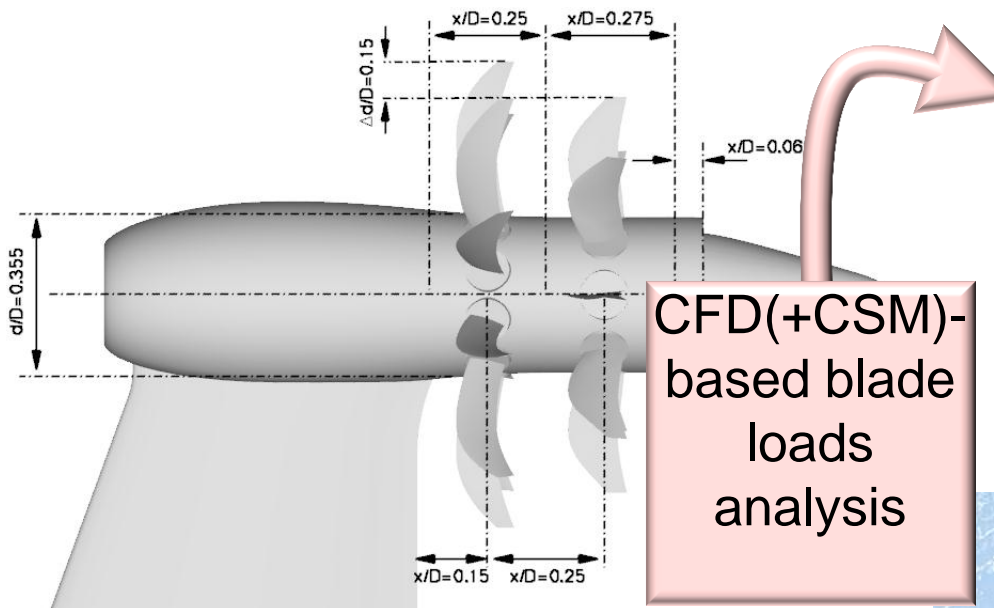
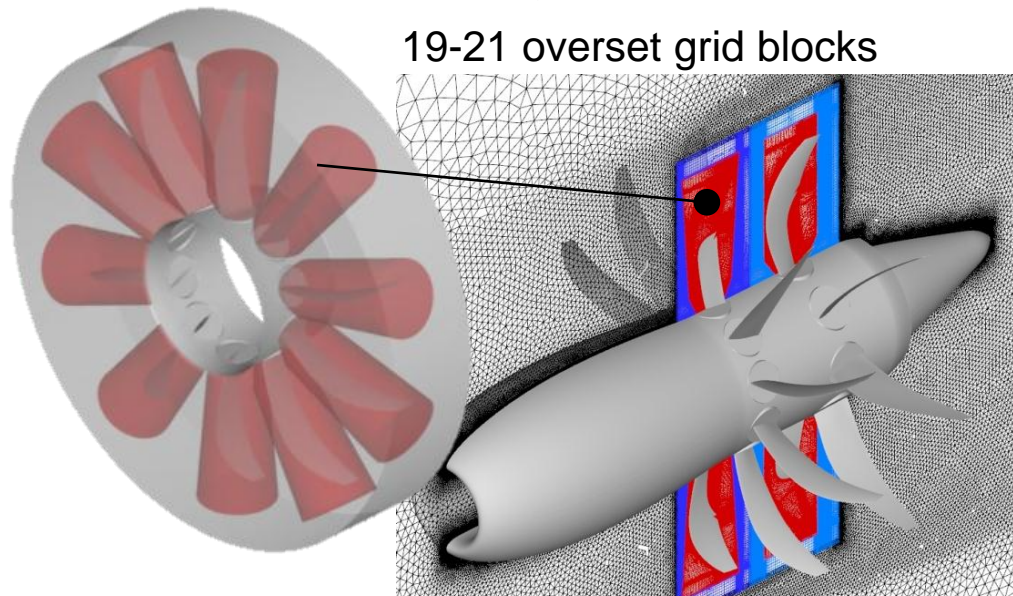


Open Rotor Applications: CROR Flow Analysis

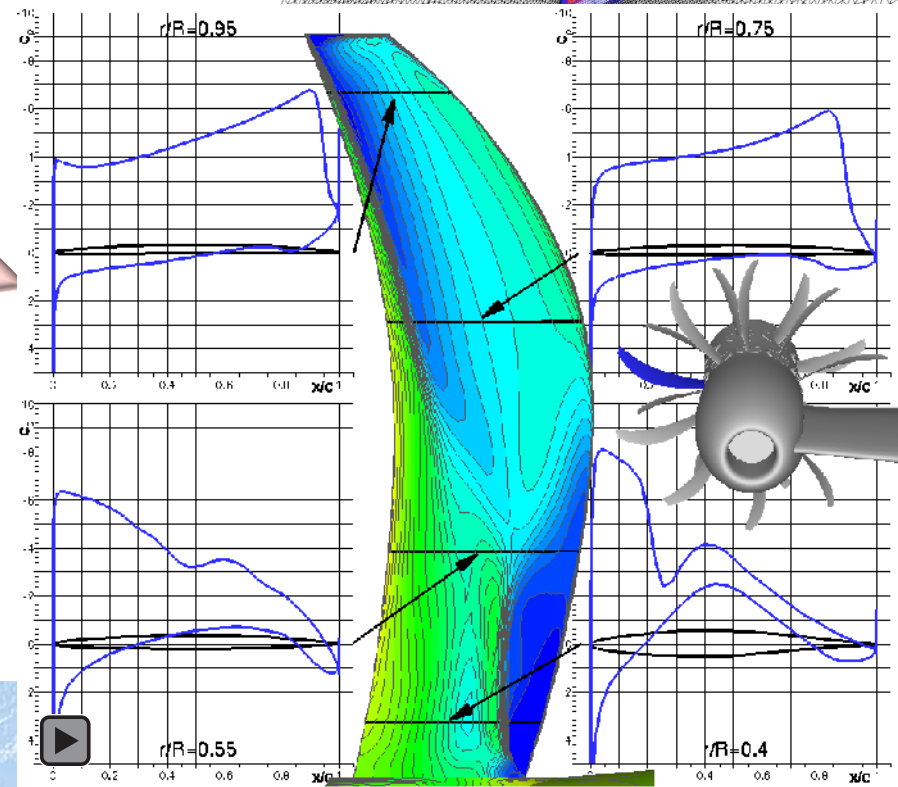
Here: Isolated rotor case

- Unstruct. background grid, struct. spinner & blade grids, „pre-generated“ holes used
- Perform. & noise analysis of many config. variations
- Comp. time: 65M nodes case, 360 procs.: 720 timesteps per revolution necessary => ~4d per rev; 6-12 revs necessary => ~1.5-3 weeks

19-21 overset grid blocks



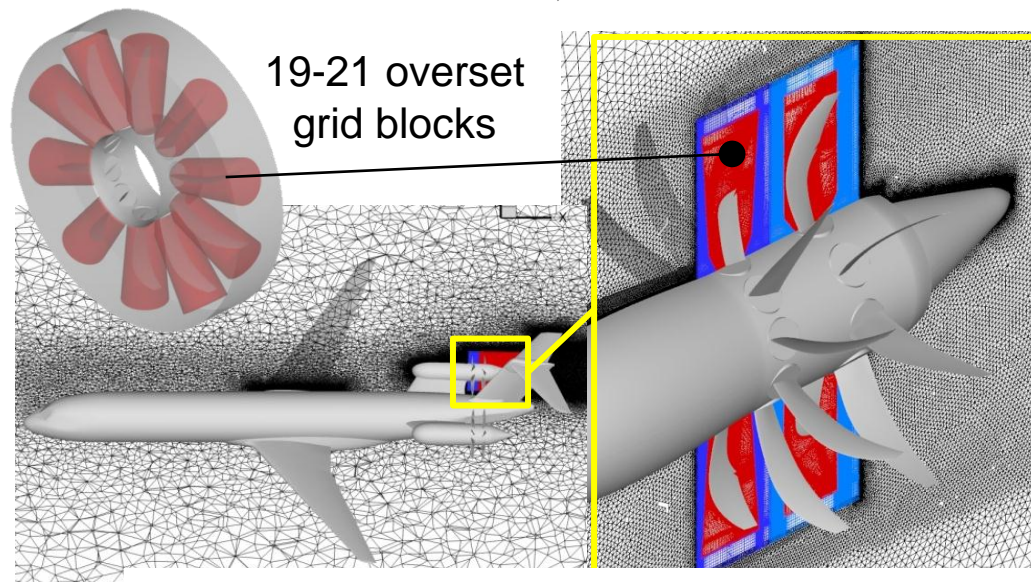
CFD(+CSM)-
based blade
loads
analysis



Open Rotor Applications: CROR Flow Analysis

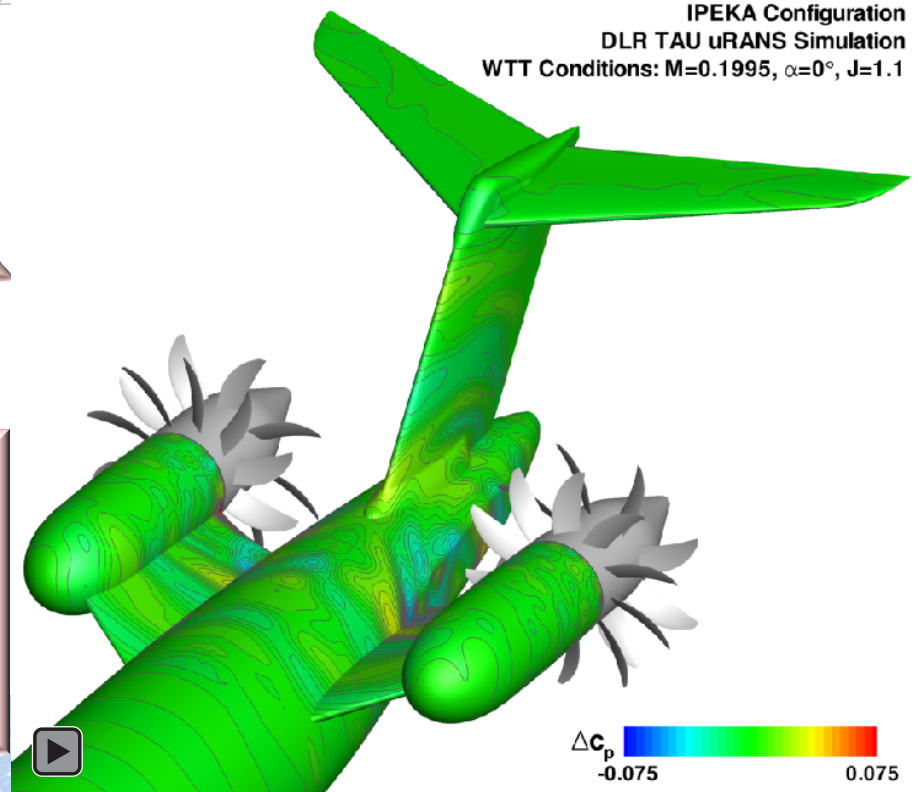
Here: Integrated rotor case

- Unstruct. background grid, struct. spinner & blade grids, „pre-generated“ holes used

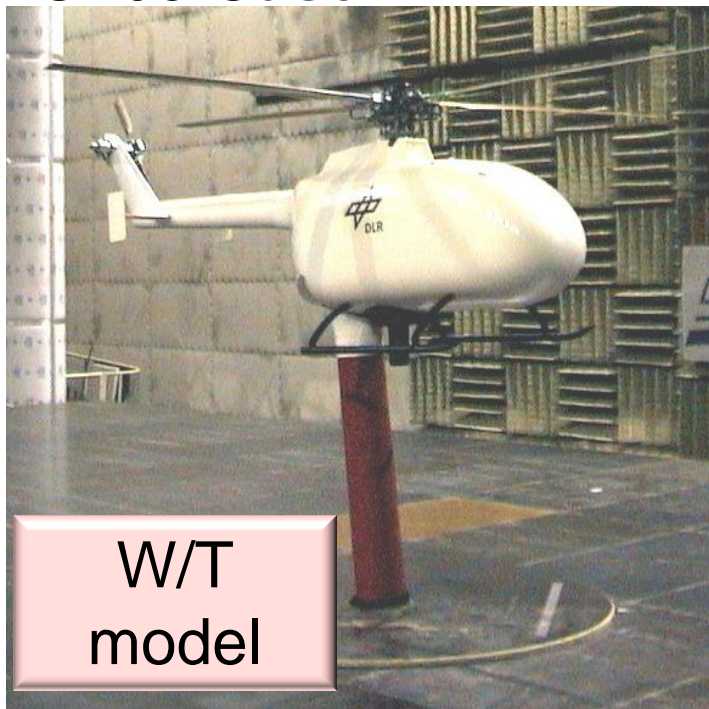


IPEKA Configuration
DLR TAU uRANS Simulation
WTT Conditions: $M=0.1995$, $\alpha=0^\circ$, $J=1.1$

CFD-based
airframe
loads
analysis



Helicopter Applications: BO105 Case



W/T
model

$$\alpha_{\text{fuselage}} = -5.2$$

$$M_{\infty} = 0.1766$$

$$M_{\text{MR}} = 0.652$$

$$M_{\text{TR}} = 0.63$$

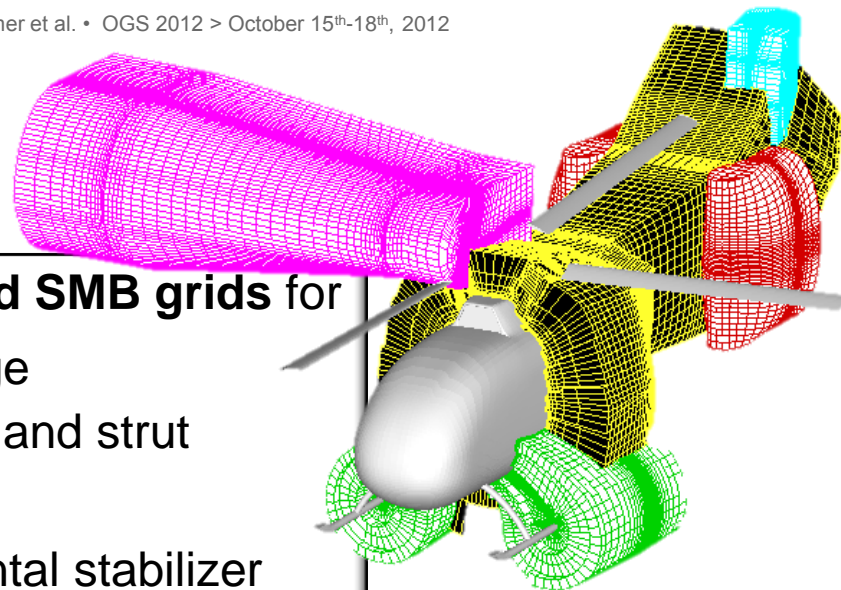
$$Q_{\text{MR}} = 10.5^{\circ} - 6.3^{\circ} \sin(Y) + 1.9^{\circ} \cos(Y)$$

$$Q_{\text{TR}} = 8.0^{\circ}$$



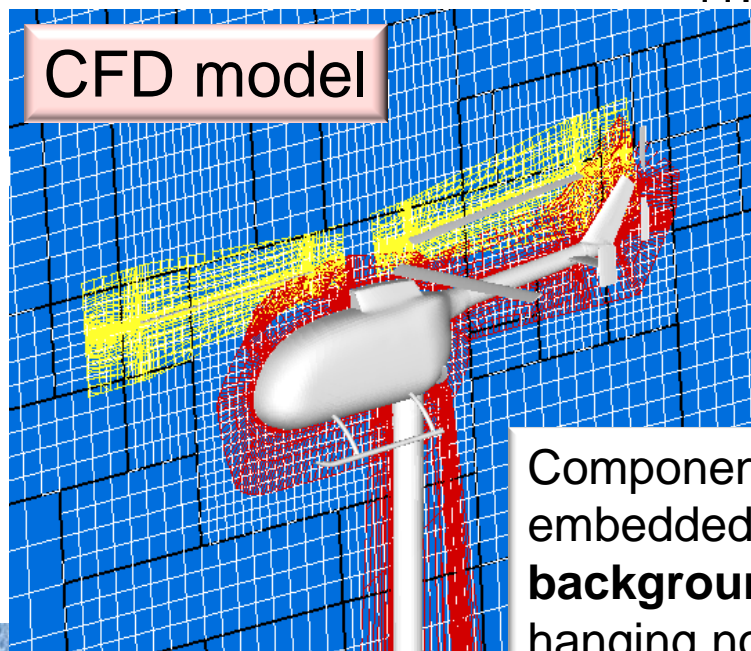
Nearfield SMB grids for

- fuselage
- spoiler and strut
- skids
- horizontal stabilizer
- main rotor and tail rotor



Total: 480 blocks,
11.8m nodes

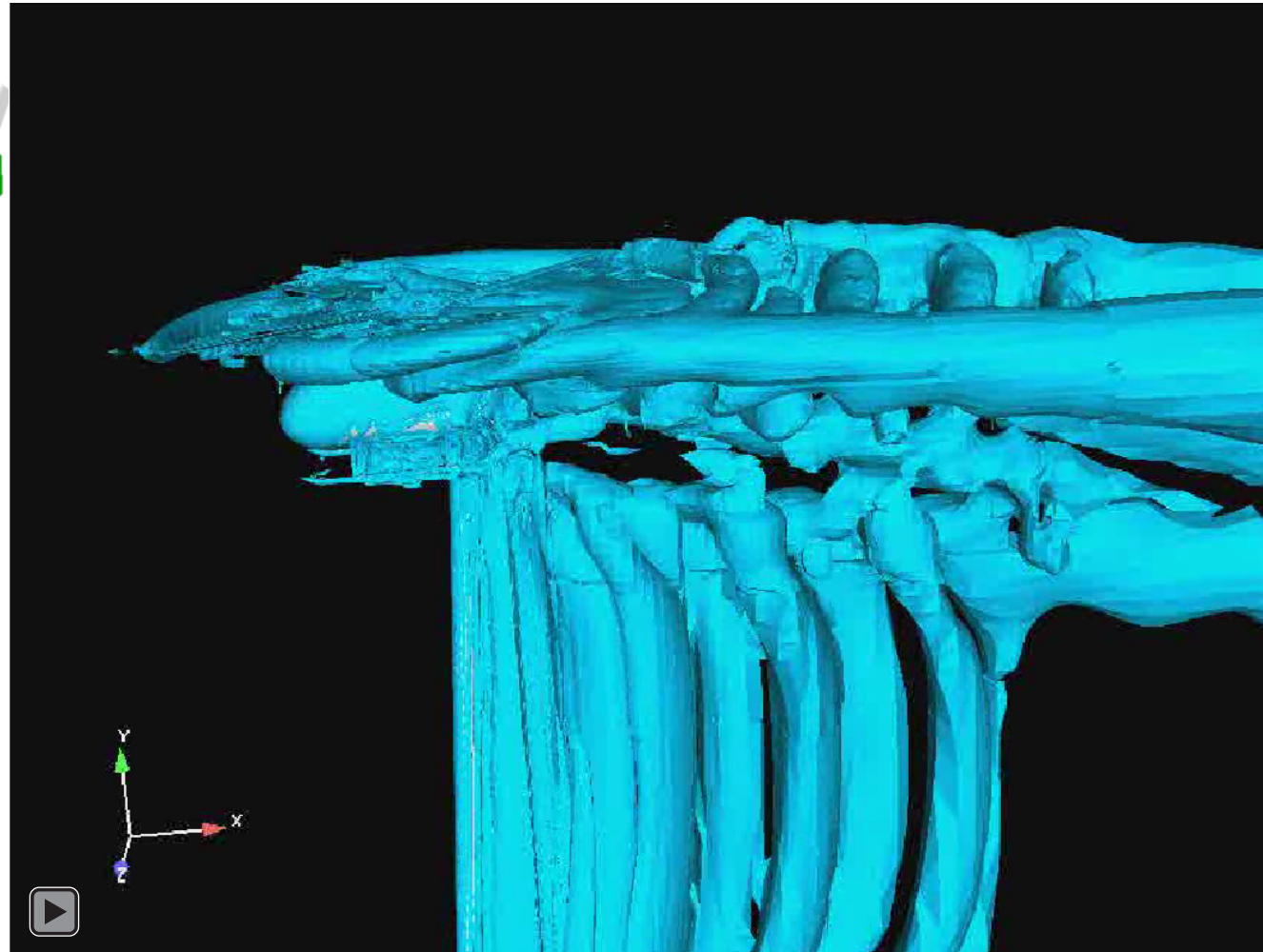
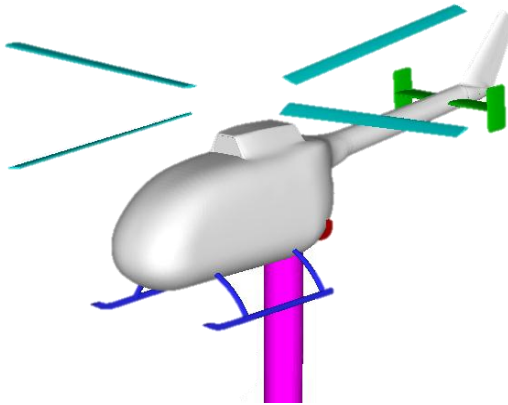
CFD model



Component grids are
embedded in **Cartesian
background grid** with
hanging nodes

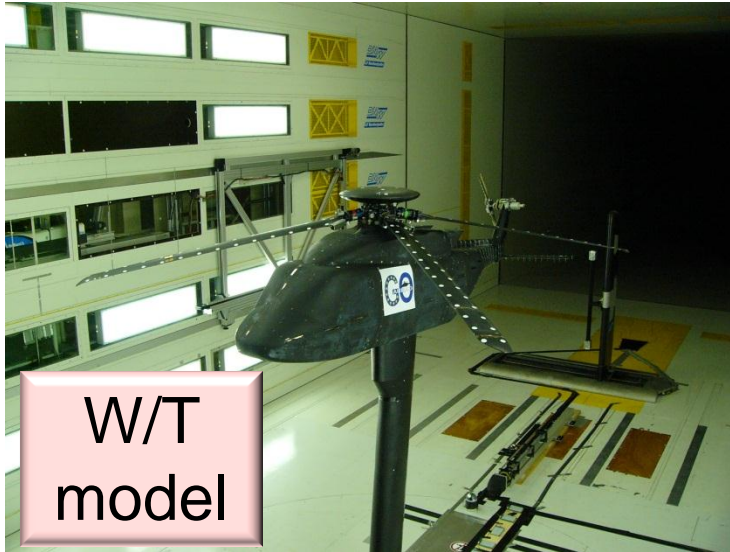
Helicopter Applications: BO105 Case

λ_2 iso-surfaces

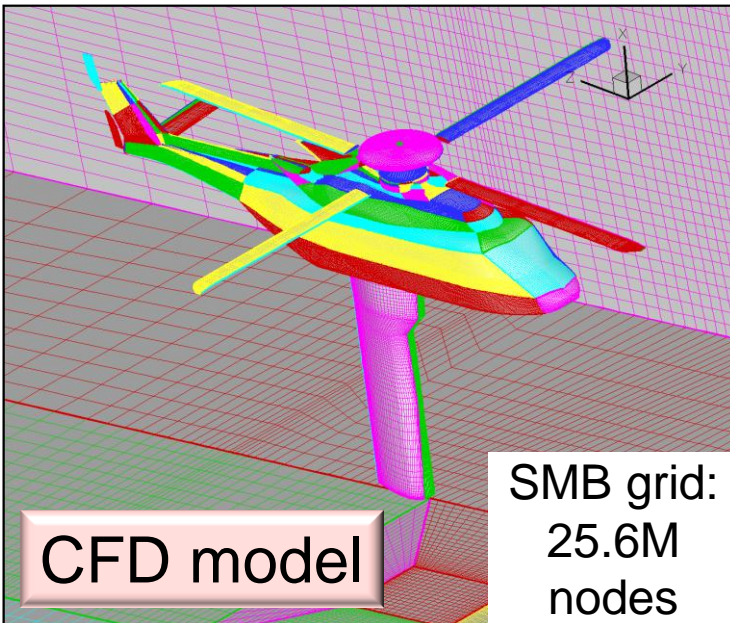
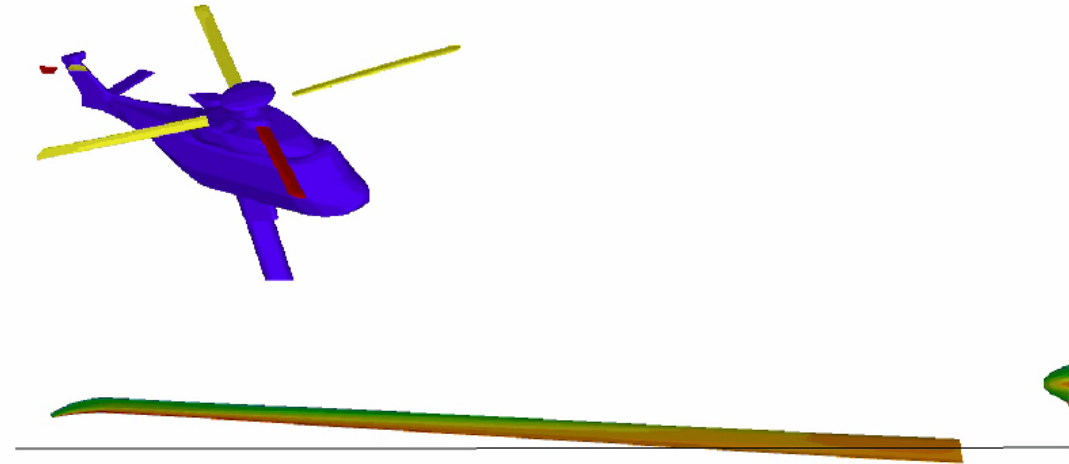


Helicopter Applications: GOAHEAD Case

FLOWer-HOST* loose coupling
=> trim + elastic blade defo. considered

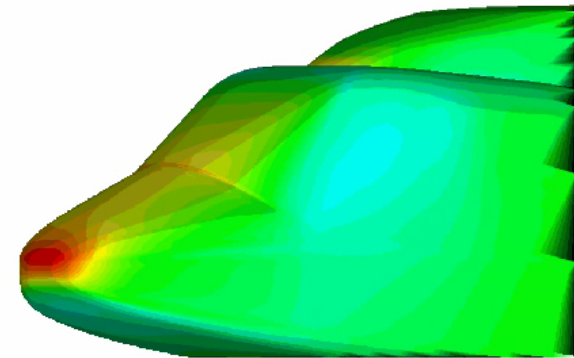


W/T
model



CFD model

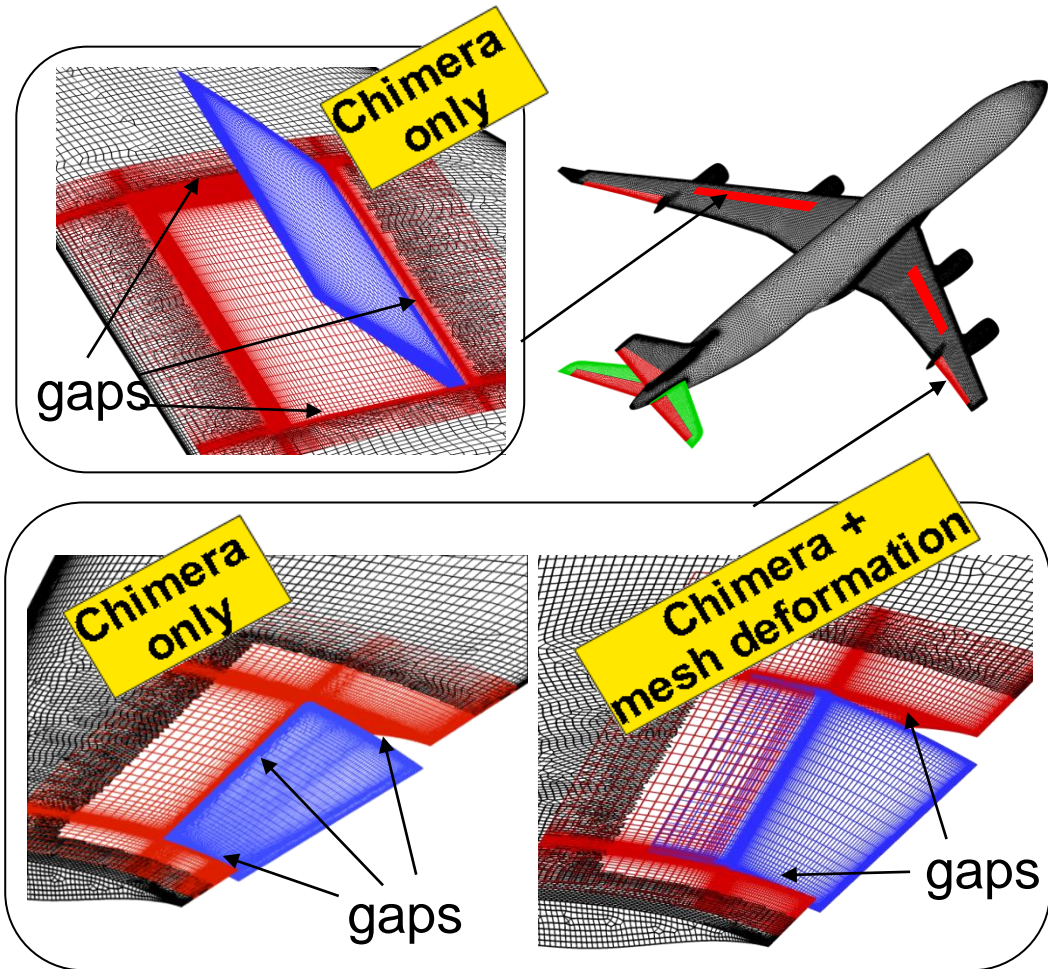
SMB grid:
25.6M
nodes



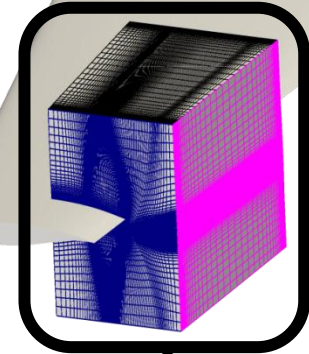
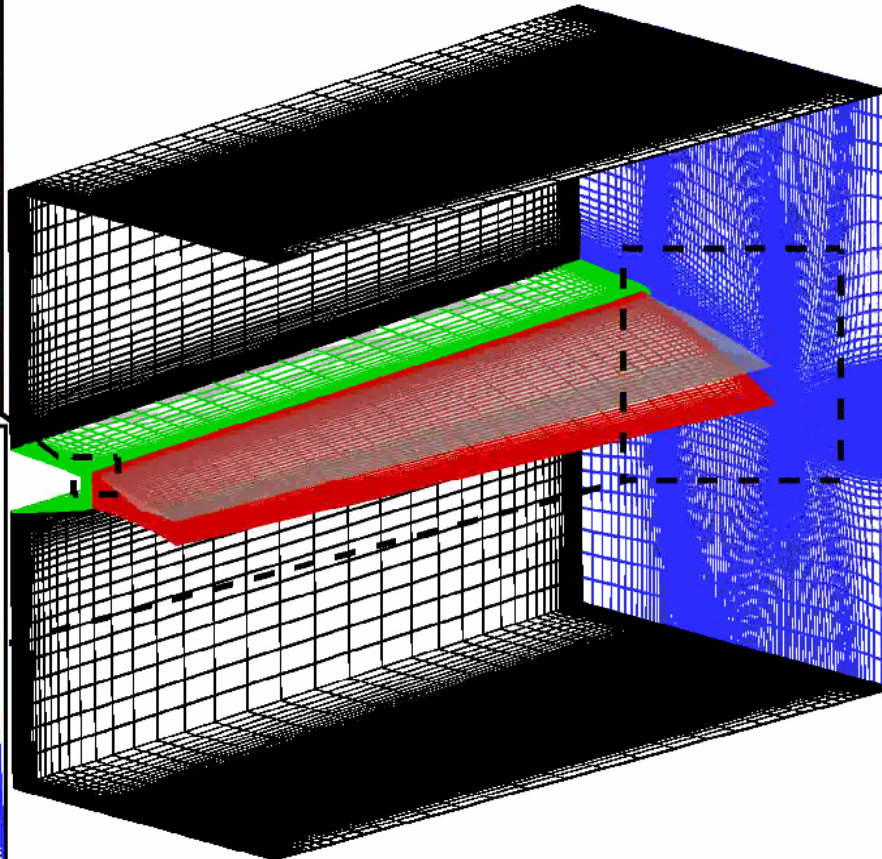
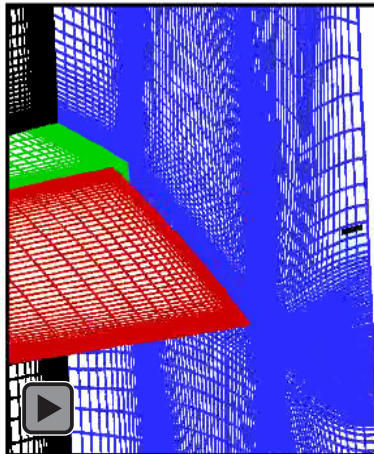
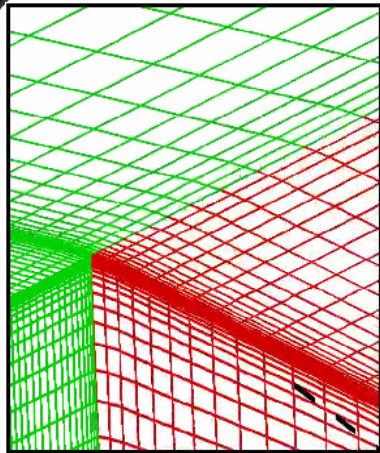
* HOST= Comprehensive analysis codes

Control Surface (CS) Motions

- Meshing & sim. of configs. with **statically deflected CS** is standard application
- Though it still challenging consideration of **moving CS** becomes more important (e.g. analysis of maneuver loads & effectiveness of gust load alleviation systems)
- Main issue: Gap handling
2 Approaches:
 - Chimera-only: Rotating Chimera block
 - Chimera+Mesh defo.: Fixed Chimera block (seems most promising)



Control Surface Motions: Overset Grid Technology + Mesh Deformation

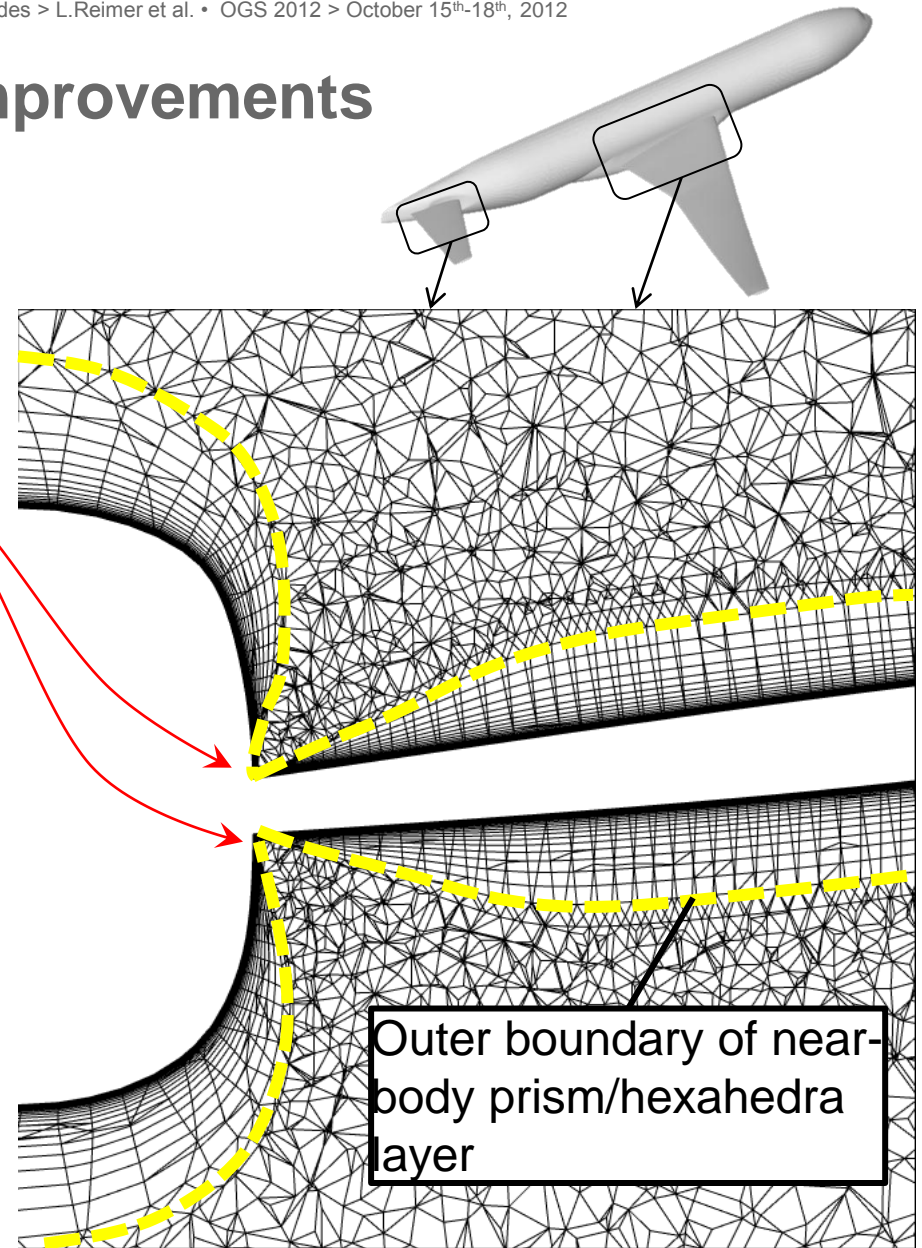


Mesh defo. only
applied to Chimera
block containing the
aileron



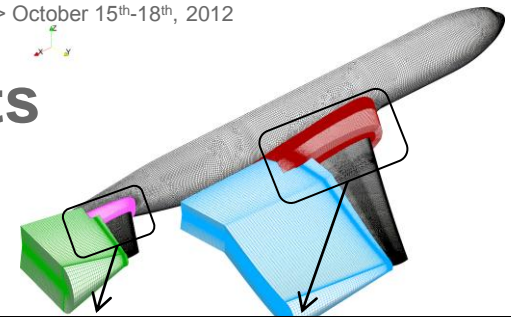
Local Discretisation Improvements Example from DPW-4

- Boundary layer in wing/HTP-fuselage junction of inappropriate quality
- Flow separations might not be detected at all or are metric driven

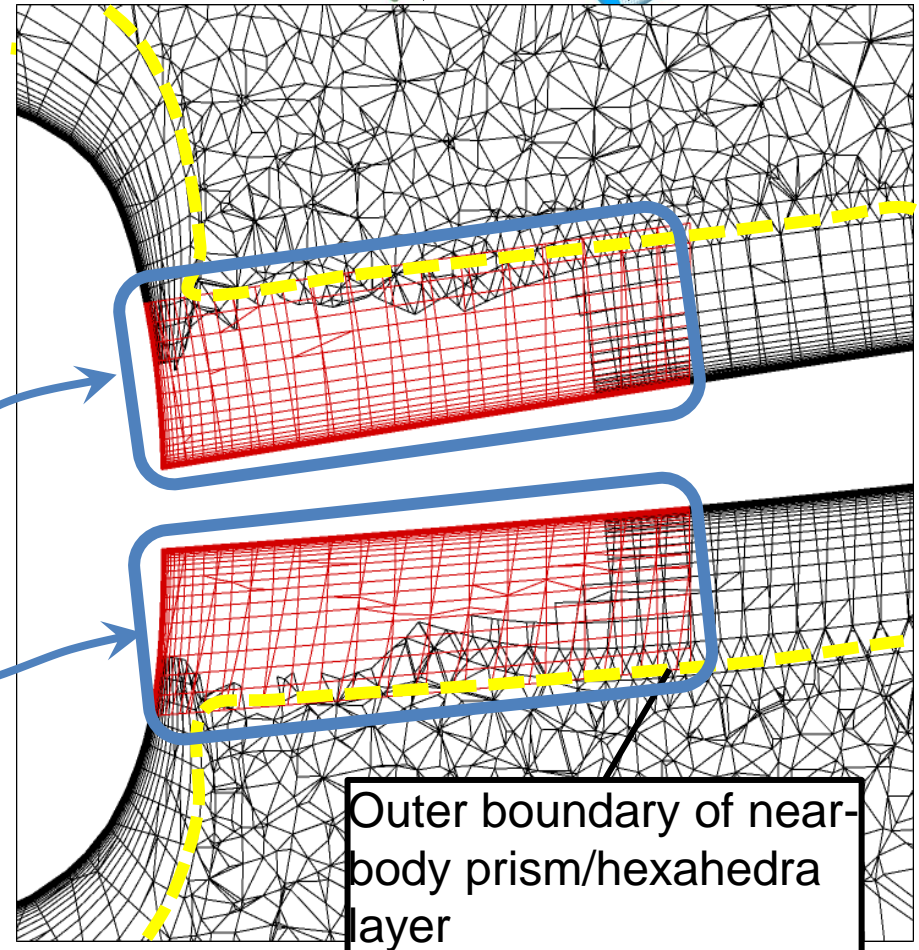


Local Discretisation Improvements

Example from DPW-4



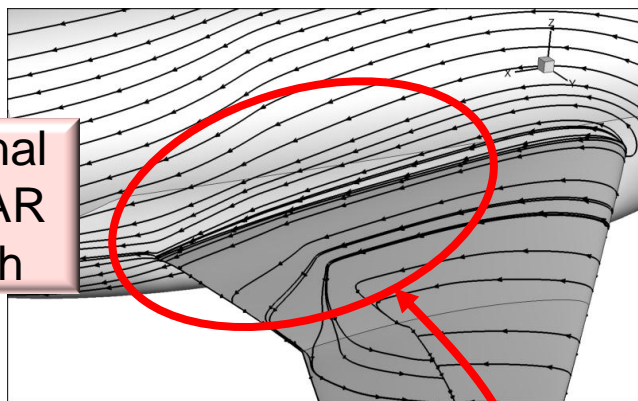
- Boundary layer in wing/HTP-fuselage junction of inappropriate quality
- Flow separations might not be detected at all or are metric driven
- Discretisation can be improved locally by inserting a structure Chimera grid



Outer boundary of near-body prism/hexahedra layer

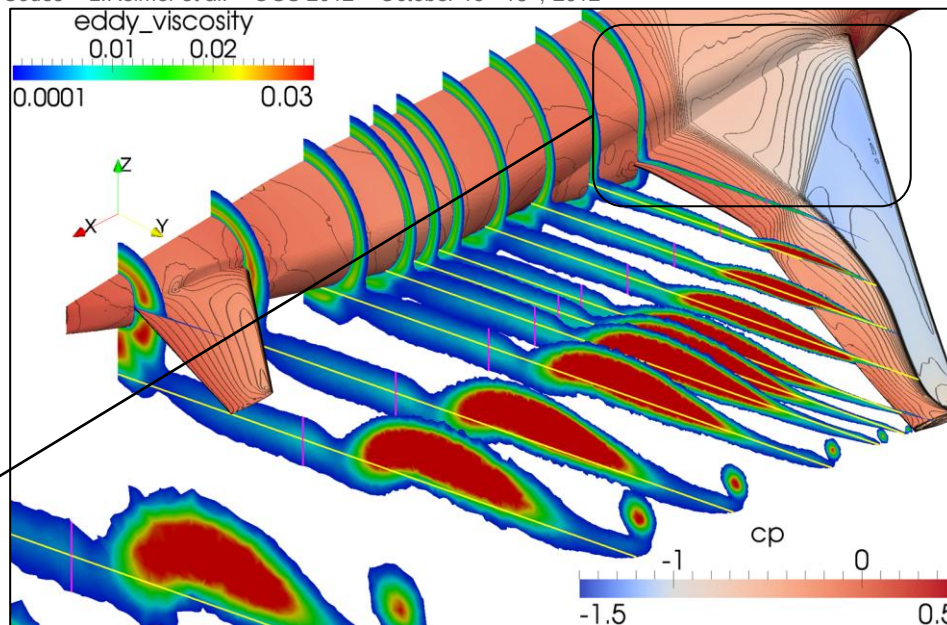
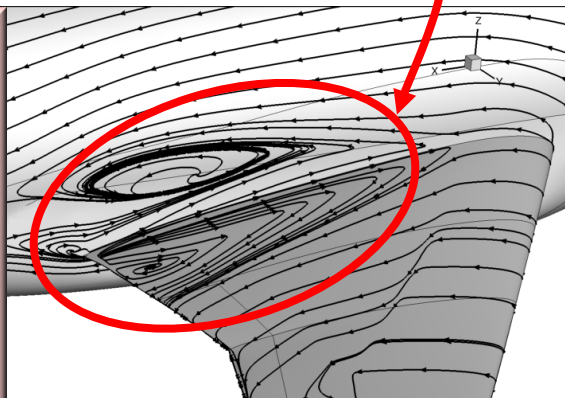
Local Discretisation Improvements Example from DPW-4

Original
SOLAR
mesh

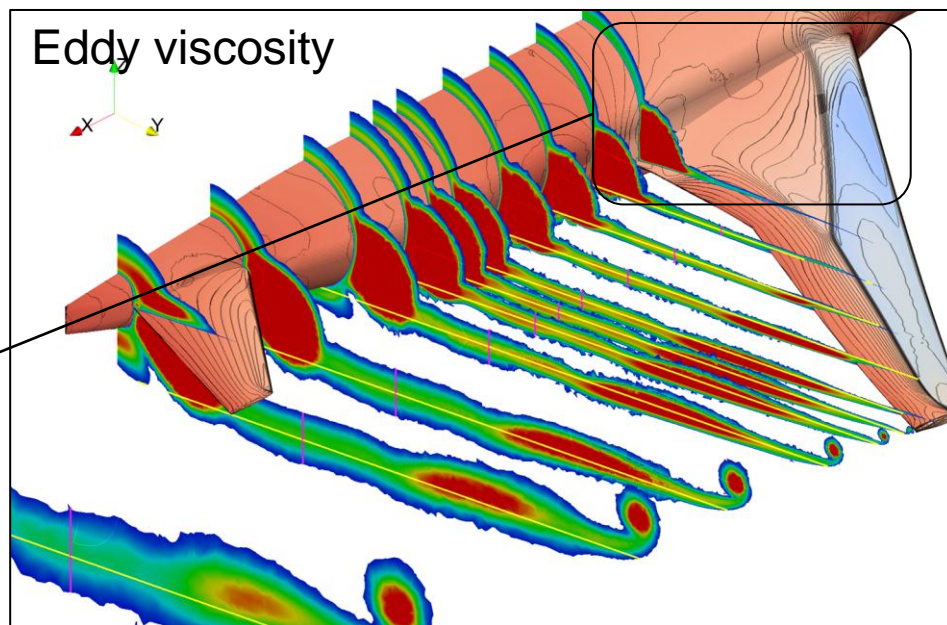


streamlines

Original
SOLAR
mesh
+
Chimera
„glove“
meshes

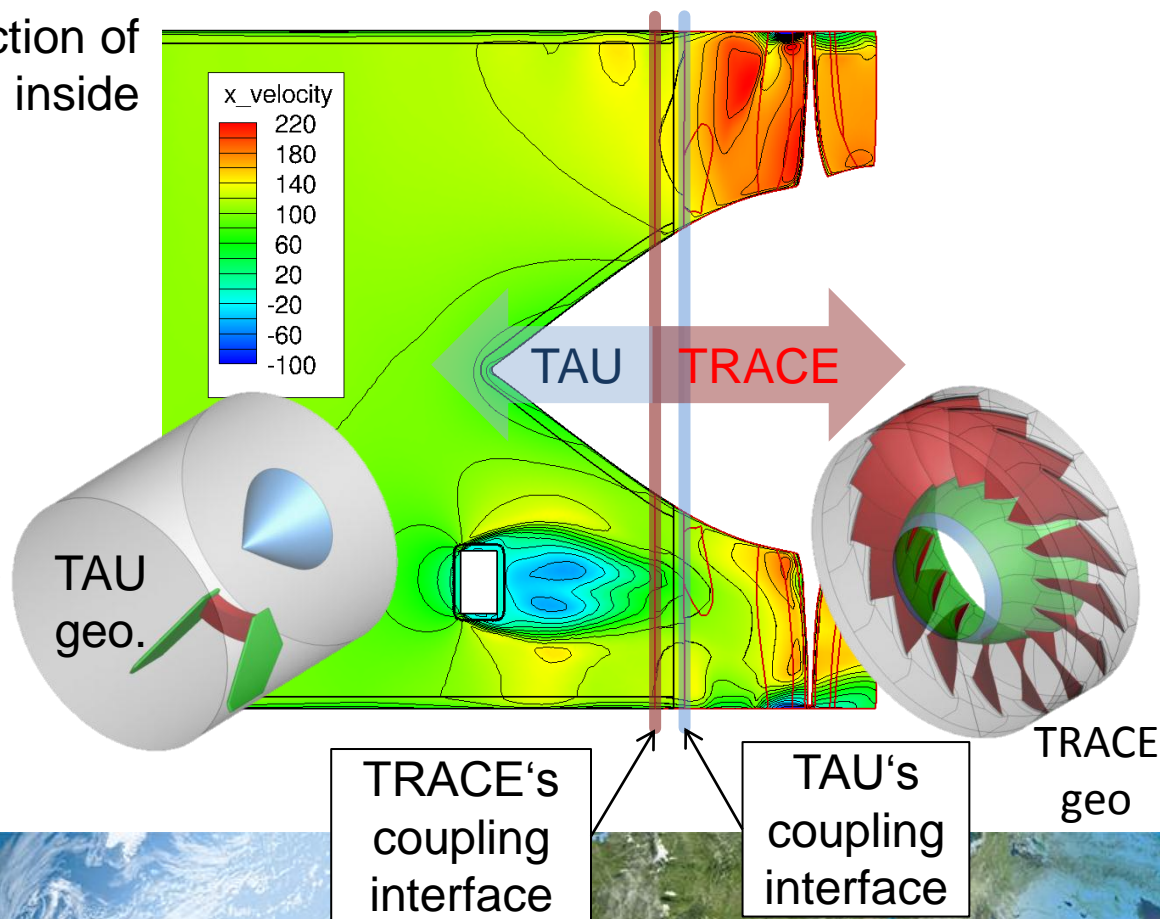
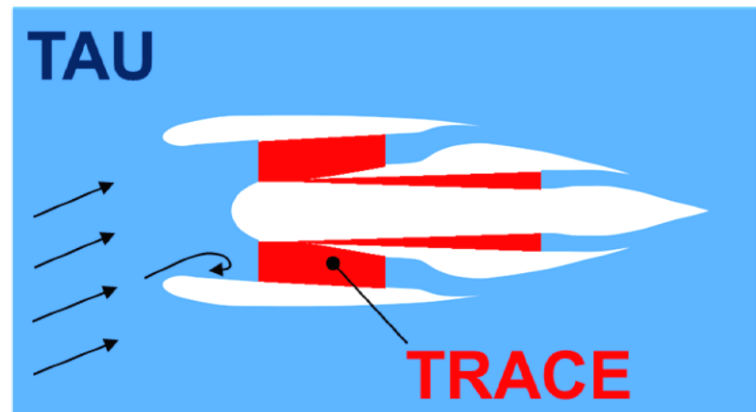


Eddy viscosity



Code-to-Code Coupling: TAU-TRACE

- **Objective:** Flow simulation of a stalling nacelle including entry of the separated flow into the engine fan
- Requires accurate flow prediction of both external flow and flow inside engine fan
- **TRACE:**
 - DLR's turbomachinery CFD code
 - Multi-block-structured
 - cell-centered code (TAU: node-centered)
- Coupling controlled by socket communication layer
- Spatial coupling with Chimera



Code-to-Code Coupling: TAU-Cartesian TAU

Problem: 2nd order spatial accuracy too dissipative for accurate computation of convection of gusts or wake vortices

Solution: Coupling of higher-order Cartesian solver (CTAU) to 2nd order solver (TAU)

Cartesian TAU:

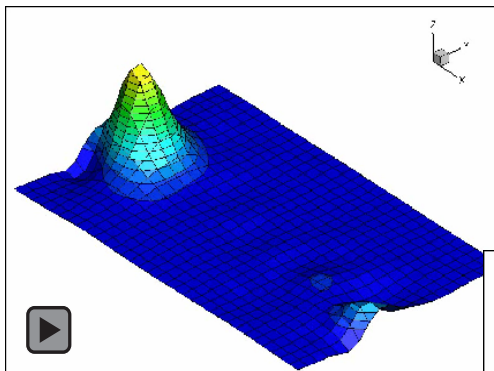
- $\geq 4^{\text{th}}$ order spatially accurate (Pade scheme)
- very coarse Cartesian meshes, easy to generate

Conventional TAU:

- 2nd order spatially accurate
- fine body-fitted hybrid meshes

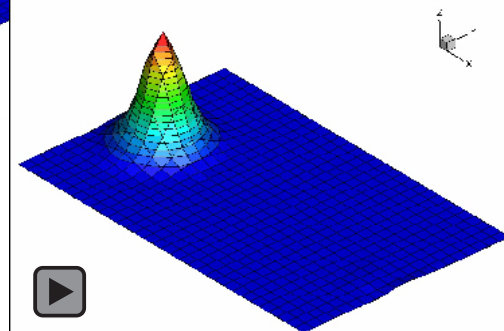
Coupling: overset grid interpolation

2nd order central

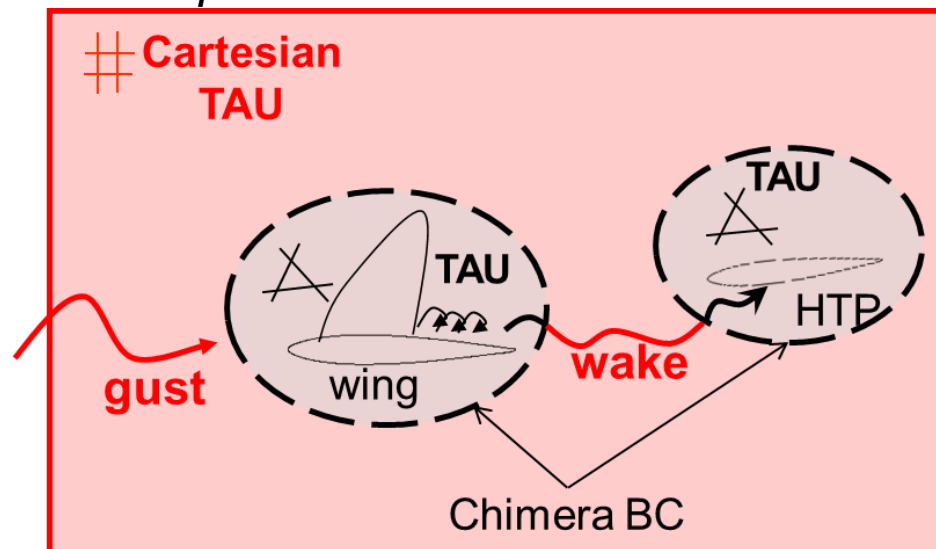


Example:
Ehrenfried vortex

4th order Pade



Concept:



Conclusions

- DLR's CFD solvers are very mature, feature standard Chimera capabilities and are thus applicable to wide range of industrially-relevant configurations that need Chimera
- Our current major problem:
 - Too many manual operations needed to setup Chimera cases
 - Lack of toolkits like CGT, etc., at DLR
 - High demand for a more „automated“ Chimera case setup process
- Since there is now a fast growing spectrum of applications that rely on the Chimera technique (Digital-X project: -> virtual flight testing), we currently increase our effort to bring forward our Chimera capabilities (e.g. overlap optimization, overlap adaptation, further development of CTAU solver, ...)

